

PROJECT : DENE ME

(DENE .ST4)

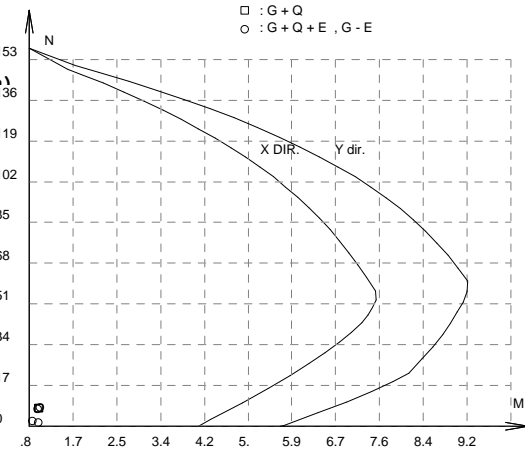
CB01 COLUMN

I/J :1/ Bx/By :25/35
 Material: E1 C25 S420

$\beta_x:1.000 \quad \beta_y:1.000 \quad Hk :3.0 \text{ m}$

□ : G+Q
 ○ : G+Q+E , G-E

COMBINATION	maxNd (t)	topMx	botMx	topMy	botMy (tm)
1. (G+G+G+G)	4.86	0.01	0.01	0.03	0.01
2. (Q+Q+Q+Q)	0.59	0.00	0.00	0.00	0.00
3. (o+Q+o+Q)	0.33	0.00	0.00	0.00	0.00
4. (Q+o+Q+o)	0.25	0.00	0.00	0.00	0.00
5. (Q+Q+o+Q)	0.46	0.00	0.00	0.00	0.00
6. (o+Q+Q+o)	0.37	0.00	0.00	0.00	0.00
7. (o+o+Q+Q)	0.33	0.00	0.00	0.00	0.00
Soil	0.07	0.00	0.00	0.00	-0.01
X-Seismic+%5	-2.14	0.04	0.05	-0.02	-0.01
X-Seismic-%5	-1.97	0.04	0.05	-0.02	-0.01
Y-Seismic+%5	-2.45	-0.01	-0.01	0.13	0.16
Y-Seismic-%5	-2.71	-0.02	-0.01	0.13	0.16
X-Wind +%5	-0.23	0.00	0.01	0.00	0.00
X-Wind -%5	-0.21	0.00	0.01	0.00	0.00
Y-Wind +%5	-0.35	0.00	0.00	0.02	0.02
Y-Wind -%5	-0.38	0.00	0.00	0.02	0.02



DESIGN :	X- (G+Q)	X- (G+Q+E)	Y- (G+Q)	Y- (G+Q+E)	X- (G-E)	Y- (G-E)
max. Nd (t) :	7.466	7.245	7.466	7.980	2.227	1.664
minor M (tm) :	0.046	0.010	0.016	-0.004	0.005	-0.005
major M (tm) :	0.168	0.163	0.190	0.203	0.056	0.176
fcd (kg/cm ²) :	166.667	166.667	166.667	166.667	166.667	166.667
μ :	0.0025	0.0025	0.0025	0.0025	0.0025	0.0025
As (cm ²) :	2.188	2.188	2.188	2.188	2.188	2.188

Cqa=0.600

REINF : 2x2ø14+2x1ø14 (web) + ø8/10(stirrup)

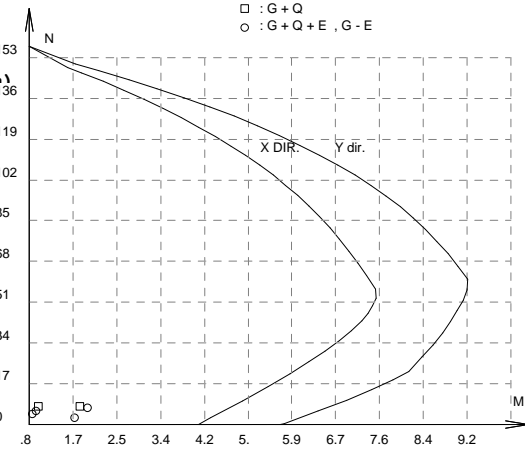
CB02 COLUMN

I/J :8/ Bx/By :25/35
 Material: E1 C25 S420

$\beta_x:1.000 \quad \beta_y:1.000 \quad Hk :3.0 \text{ m}$

□ : G+Q
 ○ : G+Q+E , G-E

COMBINATION	maxNd (t)	topMx	botMx	topMy	botMy (tm)
1. (G+G+G+G)	4.92	0.00	0.00	-0.46	-0.22
2. (Q+Q+Q+Q)	0.80	0.00	0.00	-0.18	-0.09
3. (o+Q+o+Q)	0.43	0.00	0.00	-0.20	-0.10
4. (Q+o+Q+o)	0.36	0.00	0.00	0.02	0.01
5. (Q+Q+o+Q)	0.58	0.00	0.00	-0.14	-0.07
6. (o+Q+Q+o)	0.52	0.00	0.00	-0.01	-0.01
7. (o+o+Q+Q)	0.48	0.00	0.00	-0.20	-0.10
Soil	0.01	0.00	0.00	0.00	-0.01
X-Seismic+%5	-0.15	0.05	0.06	-0.09	-0.04
X-Seismic-%5	0.13	0.06	0.06	0.06	0.03
Y-Seismic+%5	-1.09	0.00	0.00	-0.23	0.00
Y-Seismic-%5	-1.50	-0.01	0.00	-0.45	-0.11
X-Wind +%5	-0.02	0.01	0.01	-0.01	-0.01
X-Wind -%5	0.01	0.01	0.01	0.01	0.00
Y-Wind +%5	-0.15	0.00	0.00	-0.03	0.00
Y-Wind -%5	-0.21	0.00	0.00	-0.07	-0.02



DESIGN :	X- (G+Q)	X- (G+Q+E)	Y- (G+Q)	Y- (G+Q+E)	X- (G-E)	Y- (G-E)
max. Nd (t) :	7.665	5.533	7.665	6.904	4.278	2.931
minor M (tm) :	-0.663	-0.193	-0.003	-0.009	-0.243	-0.007
major M (tm) :	-0.172	0.124	-0.971	-1.118	0.058	-0.866
fcd (kg/cm ²) :	166.667	166.667	166.667	166.667	166.667	166.667
μ :	0.0025	0.0025	0.0025	0.0025	0.0025	0.0025
As (cm ²) :	2.188	2.188	2.188	2.188	2.188	2.188

Cqa=0.600

REINF : 2x2ø14+2x1ø14 (web) + ø8/10(stirrup)

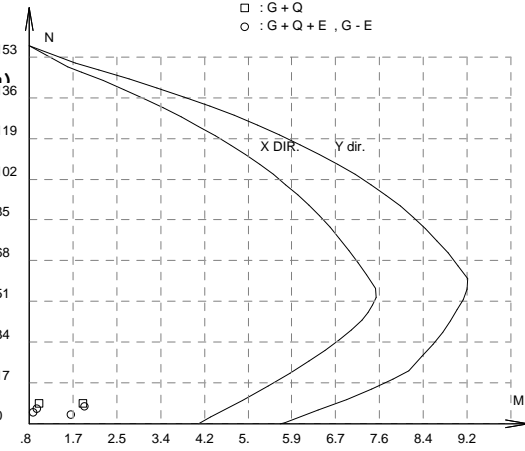
CB03 COLUMN

I/J :25/ Bx/By :25/35
 Material: E1 C25 S420

$\beta_x:1.000 \quad \beta_y:1.000 \quad Hk :3.0 \text{ m}$

□ : G+Q
 ○ : G+Q+E , G-E

COMBINATION	maxNd (t)	topMx	botMx	topMy	botMy (tm)
1. (G+G+G+G)	5.49	0.00	0.00	-0.48	-0.23
2. (Q+Q+Q+Q)	0.96	0.00	0.00	-0.19	-0.09
3. (o+Q+o+Q)	0.52	0.00	0.00	-0.21	-0.10
4. (Q+o+Q+o)	0.43	0.00	0.00	0.02	0.01
5. (Q+Q+o+Q)	0.67	0.00	0.00	-0.15	-0.07
6. (o+Q+Q+o)	0.62	0.00	0.00	-0.01	-0.01
7. (o+o+Q+Q)	0.62	0.00	0.00	-0.22	-0.11
Soil	0.00	0.00	0.00	0.00	-0.01
X-Seismic+%5	0.06	0.06	0.06	-0.05	-0.02
X-Seismic-%5	0.22	0.06	0.06	0.04	0.02
Y-Seismic+%5	-1.00	0.00	0.00	-0.23	0.00
Y-Seismic-%5	-1.24	0.00	0.00	-0.36	-0.06
X-Wind +%5	0.01	0.01	0.01	-0.01	0.00
X-Wind -%5	0.02	0.01	0.01	0.00	0.00
Y-Wind +%5	-0.14	0.00	0.00	-0.04	0.00
Y-Wind -%5	-0.17	0.00	0.00	-0.06	-0.01



DESIGN :	X- (G+Q)	X- (G+Q+E)	Y- (G+Q)	Y- (G+Q+E)	X- (G-E)	Y- (G-E)
max. Nd (t) :	8.610	6.290	8.610	7.307	4.720	3.702
minor M (tm) :	-1.013	-0.417	-0.004	-0.005	-0.471	-0.004
major M (tm) :	-0.194	0.142	-1.025	-1.057	-0.066	-0.791
fcd (kg/cm ²) :	166.667	166.667	166.667	166.667	166.667	166.667
μ :	0.0025	0.0025	0.0025	0.0025	0.0025	0.0025
As (cm ²) :	2.188	2.188	2.188	2.188	2.188	2.188

Cqa=0.600

REINF : 2x2ø14+2x1ø14 (web) + ø8/10(stirrup)

PROJECT : DENE ME

(DENE . ST4)

CB07

COLUMN

I/J :16/ Bx/By :40/

βx:1.000 βy:1.000 Hk :3.0 m

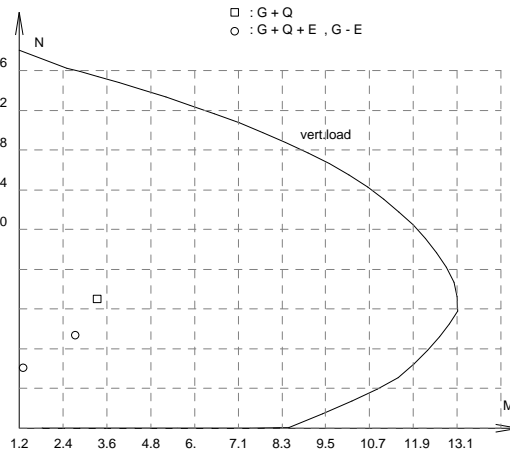
Material:E1 C25 S420

COMBINATION	maxNd (t)	topMx	botMx	topMy	botMy (tm)
1. (G+G+G+G)	43.11	-0.34	-0.17	-0.14	-0.07
2. (Q+Q+Q+Q)	12.59	-0.11	-0.05	-0.04	-0.02
3. (o+Q+o+Q)	6.07	0.07	0.04	0.16	0.08
4. (Q+o+Q+o)	6.39	-0.18	-0.09	-0.20	-0.10
5. (Q+Q+o+Q)	8.69	-0.12	-0.06	-0.06	-0.03
6. (o+Q+Q+o)	8.80	-0.14	-0.07	-0.15	-0.07
7. (o+o+Q+Q)	7.42	0.05	0.02	0.14	0.07
Soil	0.00	0.00	0.00	-0.01	-0.01
X-Seismic+%5	2.23	-0.30	-0.05	-0.09	-0.04
X-Seismic-%5	2.26	-0.37	-0.08	0.07	0.03
Y-Seismic+%5	0.94	-0.02	-0.01	-0.15	0.08
Y-Seismic-%5	0.90	0.08	0.04	-0.39	-0.03
X-Wind +%5	0.25	-0.04	-0.01	-0.01	-0.01
X-Wind -%5	0.25	-0.04	-0.01	0.01	0.00
Y-Wind +%5	0.13	0.00	0.00	-0.02	0.01
Y-Wind -%5	0.13	0.01	0.01	-0.06	-0.01

DESIGN :	X- (G+Q)	X- (G+Q+E)	Y- (G+Q)	Y- (G+Q+E)	X- (G-E)	Y- (G-E)
max. Nd (t) :	78.042	56.421	78.042	55.061	36.540	37.900
minor M (tm) :	-0.520	-0.267	-0.773	-0.445	-0.193	-0.388
major M (tm) :	-2.107	1.523	-2.107	1.487	0.061	0.269
fcd (kg/cm ²) :	166.667	166.667	166.667	166.667	166.667	166.667
μ :	0.0110	0.0110	0.0110	0.0110	0.0110	0.0110
As (cm ²) :	13.757	13.757	13.757	13.757	13.757	13.757

REINF : 9ø14 + ø8/15/5(stirrup)

Cqa=0.878



CB08

COLUMN

I/J :31/ Bx/By :40/

βx:1.000 βy:1.000 Hk :3.0 m

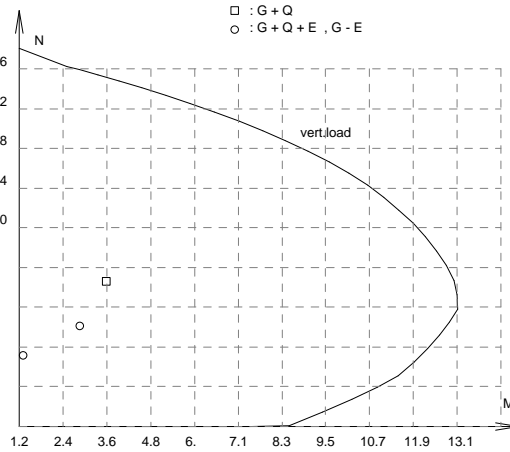
Material:E1 C25 S420

COMBINATION	maxNd (t)	topMx	botMx	topMy	botMy (tm)
1. (G+G+G+G)	47.82	0.01	0.01	-0.15	-0.07
2. (Q+Q+Q+Q)	14.70	0.00	0.00	-0.04	-0.02
3. (o+Q+o+Q)	7.32	-0.18	-0.09	0.17	0.08
4. (Q+o+Q+o)	7.23	0.18	0.09	-0.21	-0.10
5. (Q+Q+o+Q)	9.51	0.15	0.07	-0.06	-0.03
6. (o+Q+Q+o)	10.20	-0.03	-0.01	-0.16	-0.08
7. (o+o+Q+Q)	9.38	-0.12	-0.06	0.14	0.07
Soil	0.00	0.00	0.00	-0.01	-0.01
X-Seismic+%5	0.09	-0.34	-0.07	-0.03	-0.01
X-Seismic-%5	0.09	-0.42	-0.10	0.07	0.03
Y-Seismic+%5	-0.45	0.03	0.01	-0.17	0.07
Y-Seismic-%5	-0.46	0.14	0.07	-0.31	0.00
X-Wind +%5	0.01	-0.04	-0.01	0.00	0.00
X-Wind -%5	0.01	-0.05	-0.01	0.01	0.00
Y-Wind +%5	-0.06	0.00	0.00	-0.03	0.01
Y-Wind -%5	-0.06	0.02	0.01	-0.05	0.00

DESIGN :	X- (G+Q)	X- (G+Q+E)	Y- (G+Q)	Y- (G+Q+E)	X- (G-E)	Y- (G-E)
max. Nd (t) :	87.681	60.688	87.681	60.321	42.951	42.584
minor M (tm) :	-0.539	-0.422	0.295	0.330	-0.197	0.153
major M (tm) :	2.367	1.639	-2.367	1.629	0.435	-0.440
fcd (kg/cm ²) :	166.667	166.667	166.667	166.667	166.667	166.667
μ :	0.0110	0.0110	0.0110	0.0110	0.0110	0.0110
As (cm ²) :	13.757	13.757	13.757	13.757	13.757	13.757

REINF : 9ø14 + ø8/15/5(stirrup)

Cqa=0.881



CB09

COLUMN

I/J :51/ Bx/By :40/

βx:1.000 βy:1.000 Hk :3.0 m

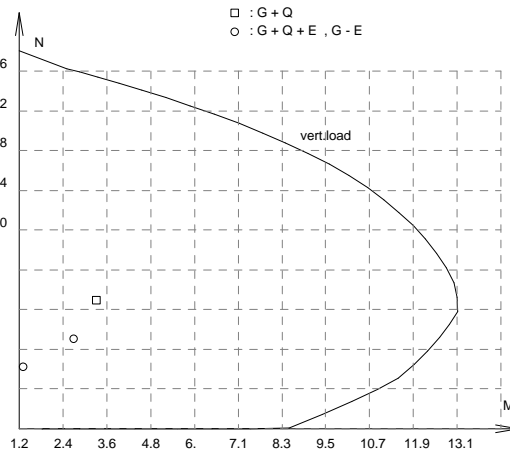
Material:E1 C25 S420

COMBINATION	maxNd (t)	topMx	botMx	topMy	botMy (tm)
1. (G+G+G+G)	42.52	0.03	0.02	0.13	0.06
2. (Q+Q+Q+Q)	12.77	0.01	0.01	0.06	0.03
3. (o+Q+o+Q)	6.48	0.19	0.09	0.16	0.08
4. (Q+o+Q+o)	6.11	-0.18	-0.09	-0.10	-0.05
5. (Q+Q+o+Q)	8.92	-0.13	-0.07	0.05	0.02
6. (o+Q+Q+o)	7.97	0.16	0.08	-0.08	-0.04
7. (o+o+Q+Q)	8.30	-0.01	0.00	0.16	0.08
Soil	0.01	0.00	0.00	-0.01	-0.01
X-Seismic+%5	-0.51	-0.38	-0.09	0.02	0.01
X-Seismic-%5	-0.61	-0.46	-0.12	0.03	0.02
Y-Seismic+%5	-9.13	0.03	0.01	0.02	0.17
Y-Seismic-%5	-8.99	0.13	0.06	0.00	0.15
X-Wind +%5	-0.05	-0.05	-0.01	0.00	0.00
X-Wind -%5	-0.06	-0.05	-0.02	0.00	0.00
Y-Wind +%5	-1.28	0.00	0.00	0.00	0.02
Y-Wind -%5	-1.26	0.02	0.01	0.00	0.02

DESIGN :	X- (G+Q)	X- (G+Q+E)	Y- (G+Q)	Y- (G+Q+E)	X- (G-E)	Y- (G-E)
max. Nd (t) :	77.600	54.427	77.600	53.202	37.652	29.133
minor M (tm) :	0.436	0.255	0.347	-0.236	0.151	0.029
major M (tm) :	2.095	1.470	2.095	1.436	-0.429	0.225
fcd (kg/cm ²) :	166.667	166.667	166.667	166.667	166.667	166.667
μ :	0.0110	0.0110	0.0110	0.0110	0.0110	0.0110
As (cm ²) :	13.757	13.757	13.757	13.757	13.757	13.757

REINF : 9ø14 + ø8/15/5(stirrup)

Cqa=0.884



PROJECT : DENE ME

(DENE . ST4)

CB16

COLUMN

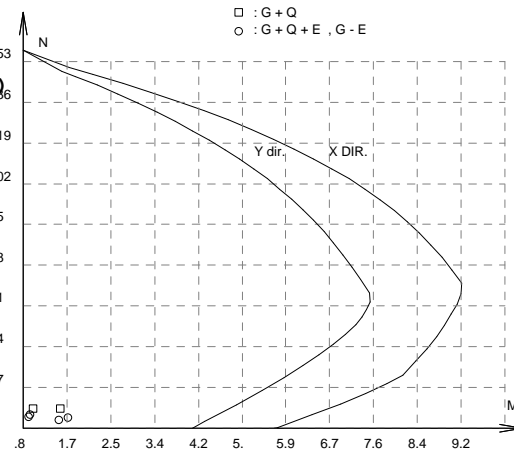
I/J :151/ Bx/By :35/25
Material:E1 C25 S420

$\beta_x:1.000 \quad \beta_y:1.000 \quad Hk :3.0 \text{ m}$

COMBINATION	maxNd (t)	topMx	botMx	topMy	botMy (tm)
1. (G+G+G+G)	5.24	0.34	0.17	0.00	0.00
2. (Q+Q+Q+Q)	0.86	0.13	0.07	0.00	0.00
3. (o+Q+o+Q)	0.45	0.10	0.05	0.00	0.00
4. (Q+o+Q+o)	0.40	0.04	0.02	0.00	0.00
5. (Q+Q+o+Q)	0.57	0.09	0.05	0.00	0.00
6. (o+Q+Q+o)	0.56	0.03	0.02	0.00	0.00
7. (o+o+Q+Q)	0.57	0.14	0.07	0.00	0.00
Soil	0.00	0.00	0.00	0.00	0.00
X-Seismic+%5	1.40	-0.37	-0.11	0.00	0.00
X-Seismic-%5	1.40	-0.37	-0.11	0.00	0.00
Y-Seismic+%5	0.00	0.00	0.00	0.10	0.10
Y-Seismic-%5	0.00	0.00	0.00	0.09	0.09
X-Wind +%5	0.15	-0.04	-0.01	0.00	0.00
X-Wind -%5	0.15	-0.04	-0.01	0.00	0.00
Y-Wind +%5	0.00	0.00	0.00	0.01	0.01
Y-Wind -%5	0.00	0.00	0.00	0.01	0.01

DESIGN :	X- (G+Q)	X- (G+Q+E)	Y- (G+Q)	Y- (G+Q+E)	X- (G-E)	Y- (G-E)
max. Nd (t) :	8.161	4.355	8.161	5.756	3.315	4.716
minor M (tm) :	0.000	0.003	0.629	0.435	-0.003	0.308
major M (tm) :	0.704	0.854	-0.184	0.130	0.679	-0.100
fcd (kg/cm ²) :	166.667	166.667	166.667	166.667	166.667	166.667
μ :	0.0025	0.0025	0.0025	0.0025	0.0025	0.0025
As (cm ²) :	2.188	2.188	2.188	2.188	2.188	2.188

REINF : 2x2ø14+2x1ø14 (web) + ø8/10 (stirrup)



CB17

COLUMN

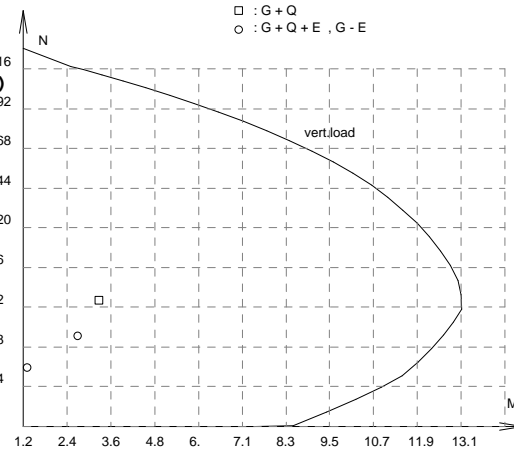
I/J :101/ Bx/By :40/

$\beta_x:1.000 \quad \beta_y:1.000 \quad Hk :3.0 \text{ m}$

COMBINATION	maxNd (t)	topMx	botMx	topMy	botMy (tm)
1. (G+G+G+G)	42.10	0.31	0.15	-0.12	-0.06
2. (Q+Q+Q+Q)	12.23	0.10	0.05	-0.03	-0.02
3. (o+Q+o+Q)	6.64	0.09	0.05	0.16	0.08
4. (Q+o+Q+o)	5.44	0.00	0.00	-0.19	-0.10
5. (Q+Q+o+Q)	8.43	0.09	0.04	-0.06	-0.03
6. (o+Q+Q+o)	8.57	0.17	0.08	-0.15	-0.07
7. (o+o+Q+Q)	7.17	-0.06	-0.03	0.14	0.07
Soil	0.00	0.00	0.00	-0.01	-0.01
X-Seismic+%5	-1.86	-0.29	-0.04	0.07	0.03
X-Seismic-%5	-2.03	-0.37	-0.08	-0.06	-0.02
Y-Seismic+%5	-0.35	-0.06	-0.03	-0.22	0.05
Y-Seismic-%5	-0.09	0.05	0.02	-0.04	0.13
X-Wind +%5	-0.21	-0.04	-0.01	0.01	0.00
X-Wind -%5	-0.23	-0.04	-0.01	-0.01	0.00
Y-Wind +%5	-0.05	-0.01	0.00	-0.03	0.01
Y-Wind -%5	-0.01	0.01	0.00	-0.01	0.02

DESIGN :	X- (G+Q)	X- (G+Q+E)	Y- (G+Q)	Y- (G+Q+E)	X- (G-E)	Y- (G-E)
max. Nd (t) :	76.141	54.884	76.141	52.502	35.860	37.544
minor M (tm) :	-0.403	-0.211	0.437	0.252	-0.165	0.222
major M (tm) :	2.056	1.482	-2.056	1.418	-0.085	-0.330
fcd (kg/cm ²) :	166.667	166.667	166.667	166.667	166.667	166.667
μ :	0.0110	0.0110	0.0110	0.0110	0.0110	0.0110
As (cm ²) :	13.757	13.757	13.757	13.757	13.757	13.757

REINF : 9ø14 + ø8/15/5 (stirrup)



CB18

COLUMN

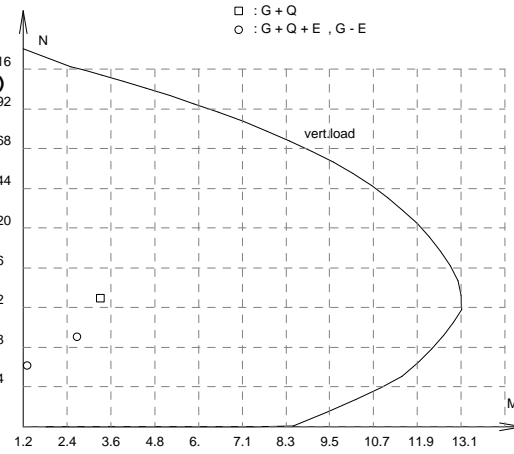
I/J :75/ Bx/By :40/

$\beta_x:1.000 \quad \beta_y:1.000 \quad Hk :3.0 \text{ m}$

COMBINATION	maxNd (t)	topMx	botMx	topMy	botMy (tm)
1. (G+G+G+G)	42.51	-0.03	-0.01	0.10	0.05
2. (Q+Q+Q+Q)	12.76	0.00	0.00	0.05	0.02
3. (o+Q+o+Q)	6.40	-0.16	-0.08	0.15	0.08
4. (Q+o+Q+o)	6.17	0.16	0.08	-0.10	-0.05
5. (Q+Q+o+Q)	9.03	0.01	0.01	0.04	0.02
6. (o+Q+Q+o)	8.61	-0.16	-0.08	-0.09	-0.04
7. (o+o+Q+Q)	7.50	0.14	0.07	0.15	0.07
Soil	0.01	0.00	0.00	-0.01	-0.01
X-Seismic+%5	1.35	-0.35	-0.07	-0.05	-0.03
X-Seismic-%5	0.47	-0.43	-0.11	-0.08	-0.04
Y-Seismic+%5	-9.25	-0.07	-0.03	-0.01	0.16
Y-Seismic-%5	-7.96	0.05	0.02	0.04	0.17
X-Wind +%5	0.14	-0.04	-0.01	0.00	0.00
X-Wind -%5	0.05	-0.05	-0.01	-0.01	0.00
Y-Wind +%5	-1.30	-0.01	0.00	0.00	0.02
Y-Wind -%5	-1.12	0.01	0.00	0.00	0.02

DESIGN :	X- (G+Q)	X- (G+Q+E)	Y- (G+Q)	Y- (G+Q+E)	X- (G-E)	Y- (G-E)
max. Nd (t) :	77.548	54.252	77.548	53.310	36.912	29.008
minor M (tm) :	0.376	0.167	-0.291	0.247	0.135	-0.042
major M (tm) :	-2.094	1.465	2.094	1.439	0.331	0.199
fcd (kg/cm ²) :	166.667	166.667	166.667	166.667	166.667	166.667
μ :	0.0110	0.0110	0.0110	0.0110	0.0110	0.0110
As (cm ²) :	13.757	13.757	13.757	13.757	13.757	13.757

REINF : 9ø14 + ø8/15/5 (stirrup)



PROJECT : DENE ME

(DENE . ST4)

CB25

COLUMN

I/J : 53/ Bx/By : 40/
Material: E1 C25 S420

βx:1.000 βy:1.000 Hk : 3.0 m

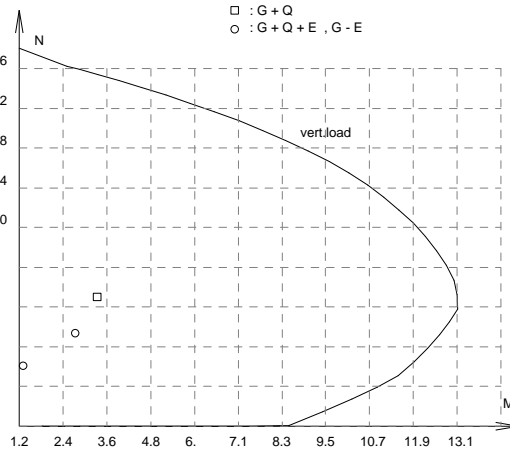
□ : G+Q
○ : G+Q+E , G-E

COMBINATION	maxNd (t)	topMx	botMx	topMy	botMy (tm)
1. (G+G+G+G)	43.10	-0.34	-0.17	0.14	0.07
2. (Q+Q+Q+Q)	12.59	-0.11	-0.05	0.04	0.02
3. (o+Q+o+Q)	6.10	0.07	0.04	0.20	0.10
4. (Q+o+Q+o)	6.36	-0.18	-0.09	-0.16	-0.08
5. (Q+Q+o+Q)	8.62	-0.12	-0.06	-0.13	-0.06
6. (o+Q+Q+o)	8.08	-0.14	-0.07	0.18	0.09
7. (o+o+Q+Q)	8.21	0.04	0.02	0.02	0.01
Soil	0.00	0.00	0.00	-0.01	-0.01
X-Seismic+%5	2.26	-0.37	-0.08	-0.07	-0.03
X-Seismic-%5	2.23	-0.30	-0.05	0.09	0.04
Y-Seismic+%5	-0.94	0.02	0.01	-0.15	0.08
Y-Seismic-%5	-0.90	-0.08	-0.04	-0.39	-0.03
X-Wind +%5	0.25	-0.04	-0.01	-0.01	0.00
X-Wind -%5	0.25	-0.04	-0.01	0.01	0.01
Y-Wind +%5	-0.13	0.00	0.00	-0.02	0.01
Y-Wind -%5	-0.13	-0.01	-0.01	-0.06	-0.01

DESIGN :	X- (G+Q)	X- (G+Q+E)	Y- (G+Q)	Y- (G+Q+E)	X- (G-E)	Y- (G-E)
max. Nd (t) :	78.033	56.415	78.033	55.055	36.536	37.896
minor M (tm) :	-0.076	-0.096	-0.367	-0.194	0.194	-0.388
major M (tm) :	-2.107	1.523	2.107	1.486	0.061	-0.269
fcd (kg/cm ²) :	166.667	166.667	166.667	166.667	166.667	166.667
μ :	0.0110	0.0110	0.0110	0.0110	0.0110	0.0110
As (cm ²) :	13.757	13.757	13.757	13.757	13.757	13.757

Cqa=0.878

REINF : 9ø14 + ø8/15/5(stirrup)



CB26

COLUMN

I/J : 77/ Bx/By : 40/
Material: E1 C25 S420

βx:1.000 βy:1.000 Hk : 3.0 m

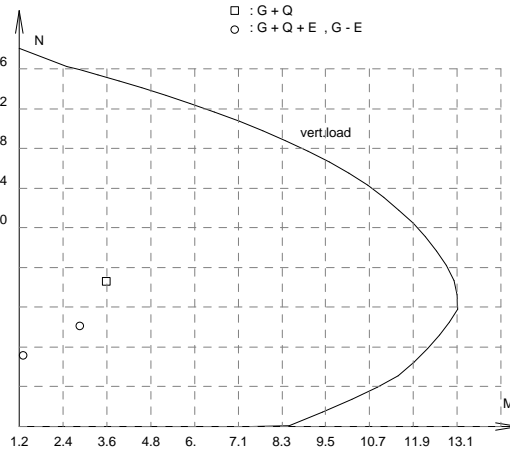
□ : G+Q
○ : G+Q+E , G-E

COMBINATION	maxNd (t)	topMx	botMx	topMy	botMy (tm)
1. (G+G+G+G)	47.82	0.01	0.01	0.15	0.07
2. (Q+Q+Q+Q)	14.70	0.00	0.00	0.04	0.02
3. (o+Q+o+Q)	7.39	-0.18	-0.09	0.21	0.10
4. (Q+o+Q+o)	7.16	0.18	0.09	-0.17	-0.08
5. (Q+Q+o+Q)	9.42	0.15	0.07	-0.14	-0.07
6. (o+Q+Q+o)	9.45	-0.03	-0.02	0.19	0.09
7. (o+o+Q+Q)	10.22	-0.12	-0.06	0.03	0.01
Soil	0.00	0.00	0.00	-0.01	-0.01
X-Seismic+%5	0.09	-0.42	-0.10	-0.07	-0.03
X-Seismic-%5	0.09	-0.34	-0.07	0.03	0.01
Y-Seismic+%5	0.45	-0.03	-0.01	-0.17	0.07
Y-Seismic-%5	0.46	-0.14	-0.07	-0.31	0.00
X-Wind +%5	0.01	-0.05	-0.01	-0.01	0.00
X-Wind -%5	0.01	-0.04	-0.01	0.00	0.00
Y-Wind +%5	0.06	0.00	0.00	-0.03	0.01
Y-Wind -%5	0.06	-0.02	-0.01	-0.05	0.00

DESIGN :	X- (G+Q)	X- (G+Q+E)	Y- (G+Q)	Y- (G+Q+E)	X- (G-E)	Y- (G-E)
max. Nd (t) :	87.676	60.684	87.676	60.317	42.948	42.582
minor M (tm) :	-0.063	0.045	-0.266	-0.023	0.197	0.153
major M (tm) :	2.367	1.638	2.367	1.629	0.435	0.440
fcd (kg/cm ²) :	166.667	166.667	166.667	166.667	166.667	166.667
μ :	0.0110	0.0110	0.0110	0.0110	0.0110	0.0110
As (cm ²) :	13.757	13.757	13.757	13.757	13.757	13.757

Cqa=0.881

REINF : 9ø14 + ø8/15/5(stirrup)



CB27

COLUMN

I/J : 103/ Bx/By : 40/
Material: E1 C25 S420

βx:1.000 βy:1.000 Hk : 3.0 m

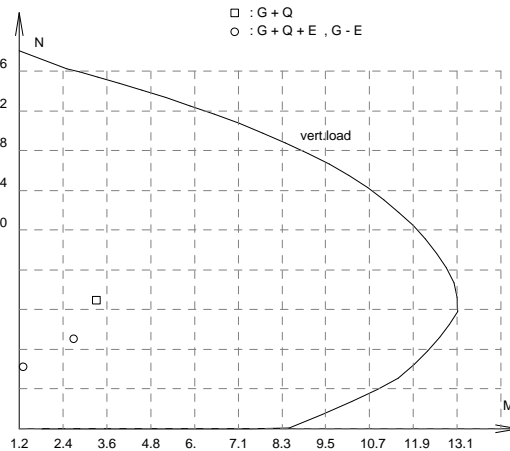
□ : G+Q
○ : G+Q+E , G-E

COMBINATION	maxNd (t)	topMx	botMx	topMy	botMy (tm)
1. (G+G+G+G)	42.51	0.03	0.02	-0.13	-0.06
2. (Q+Q+Q+Q)	12.77	0.01	0.01	-0.06	-0.03
3. (o+Q+o+Q)	6.91	0.19	0.09	-0.06	-0.03
4. (Q+o+Q+o)	5.68	-0.18	-0.09	0.00	0.00
5. (Q+Q+o+Q)	8.88	-0.13	-0.07	-0.14	-0.07
6. (o+Q+Q+o)	7.50	0.16	0.08	0.09	0.05
7. (o+o+Q+Q)	8.80	0.00	0.00	-0.08	-0.04
Soil	-0.01	0.00	0.00	-0.01	-0.01
X-Seismic+%5	-0.61	-0.46	-0.12	-0.03	-0.02
X-Seismic-%5	-0.51	-0.38	-0.09	-0.02	-0.01
Y-Seismic+%5	9.13	-0.03	-0.01	0.02	0.17
Y-Seismic-%5	8.99	-0.13	-0.06	0.00	0.15
X-Wind +%5	-0.06	-0.05	-0.02	0.00	0.00
X-Wind -%5	-0.05	-0.05	-0.01	0.00	0.00
Y-Wind +%5	1.28	0.00	0.00	0.00	0.02
Y-Wind -%5	1.26	-0.02	-0.01	0.00	0.02

DESIGN :	X- (G+Q)	X- (G+Q+E)	Y- (G+Q)	Y- (G+Q+E)	X- (G-E)	Y- (G-E)
max. Nd (t) :	77.584	54.417	77.584	53.192	37.649	29.130
minor M (tm) :	-0.286	-0.162	-0.176	-0.561	-0.151	0.029
major M (tm) :	2.095	1.469	-2.095	1.436	-0.429	-0.225
fcd (kg/cm ²) :	166.667	166.667	166.667	166.667	166.667	166.667
μ :	0.0110	0.0110	0.0110	0.0110	0.0110	0.0110
As (cm ²) :	13.757	13.757	13.757	13.757	13.757	13.757

Cqa=0.884

REINF : 9ø14 + ø8/15/5(stirrup)



PROJECT : DENE ME

(DENE . ST4)

CB34

COLUMN

I/J :76/ Bx/By :/

β_x :1.000 β_y :1.000 Hk :3.0 m

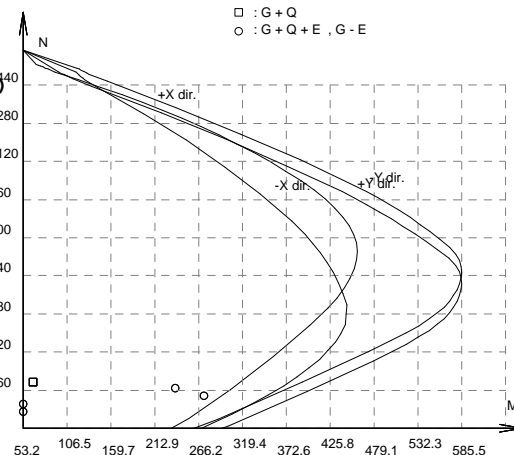
Material:E1 C25 S420

COMBINATION	maxNd (t)	topMx	botMx	topMy	botMy (tm)
1. (G+G+G+G)	114.19	-0.80	-0.20	0.01	0.00
2. (Q+Q+Q+Q)	25.44	-0.19	-0.05	0.00	0.00
3. (o+Q+o+Q)	11.48	0.76	0.21	-0.46	-0.05
4. (Q+o+Q+o)	11.35	-0.89	-0.24	0.46	0.05
5. (Q+Q+o+Q)	14.92	-0.89	-0.24	0.42	0.04
6. (o+Q+Q+o)	14.75	0.79	0.22	0.34	0.04
7. (o+o+Q+Q)	15.99	-0.16	-0.04	-0.75	-0.08
Soil	0.01	-0.15	-0.39	-0.30	-0.97
X-Seismic+%5	-33.34	-168.99	-35.83	-1.77	-0.48
X-Seismic-%5	-33.34	-168.99	-35.83	1.77	0.48
Y-Seismic+%5	0.00	0.00	0.00	-203.72	-6.70
Y-Seismic-%5	0.00	0.00	0.00	-208.90	-8.11
X-Wind +%5	-3.57	-19.74	-4.32	-0.22	-0.06
X-Wind -%5	-3.57	-19.74	-4.32	0.22	0.06
Y-Wind +%5	0.00	0.00	0.00	-30.54	-1.20
Y-Wind -%5	0.00	0.00	0.00	-31.38	-1.42

DESIGN : X- (G+Q) X- (G+Q+E) Y- (G+Q) Y- (G+Q+E) X- (G-E) Y- (G-E) M Shearwall base moment

max. Nd (t) :	194.961	169.469	194.961	136.124	69.425	102.770	Mxu: 184.2
minor M (tm) :	0.458	2.119	-0.736	-1.693	1.781	-0.720	Mxa: 184.2
major M (tm) :	-11.844	184.220	12.283	219.150	-169.708	208.911	Myu: 219.1
fcd (kg/cm ²) :	166.667	166.667	166.667	166.667	166.667	166.667	Mya: 219.1
μ :	0.0083	0.0083	0.0083	0.0083	0.0083	0.0083	
As (cm ²) :	75.695	75.695	75.695	75.695	75.695	75.695	Cqa=0.862

REINF :15 ϕ 12+42 ϕ 14 + ϕ 10/15(stirrup)



CB35

COLUMN

I/J :102/ Bx/By :25/165

β_x :1.000 β_y :1.000 Hk :3.0 m

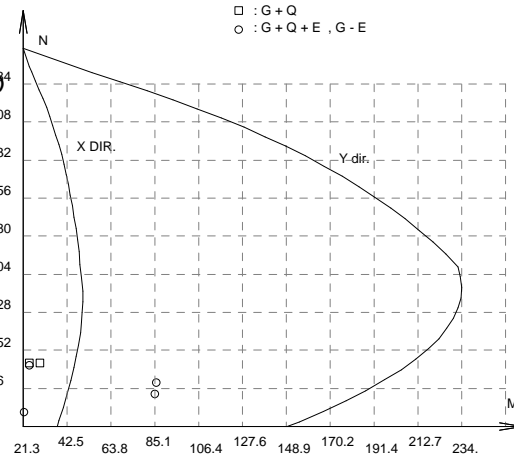
Material:E1 C25 S420

COMBINATION	maxNd (t)	topMx	botMx	topMy	botMy (tm)
1. (G+G+G+G)	71.71	-0.26	-0.13	0.00	0.00
2. (Q+Q+Q+Q)	18.51	-0.09	-0.04	0.00	0.00
3. (o+Q+o+Q)	8.76	-0.15	-0.07	-0.59	-0.16
4. (Q+o+Q+o)	8.52	0.05	0.03	0.59	0.16
5. (Q+Q+o+Q)	11.05	-0.08	-0.04	0.55	0.15
6. (o+Q+Q+o)	12.29	-0.16	-0.08	0.05	0.01
7. (o+o+Q+Q)	11.20	0.05	0.03	-0.61	-0.16
Soil	-0.01	-0.01	-0.01	-0.12	-0.31
X-Seismic+%5	35.10	-0.68	-0.16	4.73	1.23
X-Seismic-%5	35.10	-0.68	-0.16	-4.73	-1.23
Y-Seismic+%5	0.00	0.00	0.00	-63.83	-8.82
Y-Seismic-%5	0.00	0.00	0.00	-49.97	-5.21
X-Wind +%5	3.77	-0.08	-0.02	0.56	0.15
X-Wind -%5	3.77	-0.08	-0.02	-0.56	-0.15
Y-Wind +%5	0.00	0.00	0.00	-9.60	-1.39
Y-Wind -%5	0.00	0.00	0.00	-7.46	-0.83

DESIGN : X- (G+Q) X- (G+Q+E) Y- (G+Q) Y- (G+Q+E) X- (G-E) Y- (G-E) M Shearwall base moment

max. Nd (t) :	126.124	122.891	126.124	87.791	29.435	64.536	
minor M (tm) :	-0.023	4.791	-0.287	-0.207	4.734	-0.234	
major M (tm) :	-2.838	2.765	8.135	-64.431	0.443	63.830	
fcd (kg/cm ²) :	166.667	166.667	166.667	166.667	166.667	166.667	
μ :	0.0025	0.0025	0.0025	0.0025	0.0025	0.0025	
As (cm ²) :	10.313	10.313	10.313	10.313	10.313	10.313	Cqa=0.869

REINF :2x4 ϕ 20+2x7 ϕ 14 (web) + ϕ 8/12/9(stirrup)

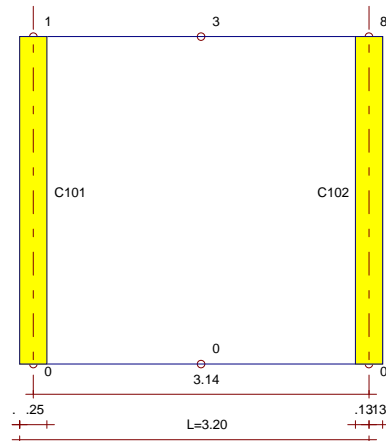


β_x, β_y : Column moment magnification factor A4 : A4 Irregularity (Ba=Bax+0.3*Bay, Ba=0.3*Bax+Bay)
 Cx, Cy : Strong column magnification factor
 Ck : Column support beam magnification factor

PB13 PANEL

I/K:1/0 Io/Jo:3/0 J/L:8/ Bx/By :282.6/25. Hk :3.0 m Cqa=1.000

COMBINATION	maxNd	upMx	dwMx	upMy	dwMy	Tx	Ty
1. (G+G+G+G)	30.38	0.16	0.04	0.00	0.00	0.07	0.00
2. (Q+Q+Q+Q)	4.37	-0.69	0.12	0.00	0.00	-0.19	0.00
3. (o+Q+o+Q)	2.43	-0.34	0.03	0.00	0.00	-0.10	0.00
4. (Q+o+Q+o)	1.88	-0.35	0.09	0.00	0.00	-0.09	0.00
5. (Q+Q+o+Q)	3.27	-0.37	0.10	0.00	0.00	-0.09	0.00
6. (o+Q+Q+o)	2.76	-0.52	0.05	0.00	0.00	-0.16	0.00
7. (o+o+Q+Q)	2.60	-0.48	0.09	0.00	0.00	-0.13	0.00
Soil	0.19	-0.29	-0.73	0.00	-0.01	-0.34	0.00
X-Seismic+%5	-5.74	11.73	27.67	0.00	0.01	13.13	0.00
X-Seismic-%5	-4.22	12.52	29.36	0.00	-0.01	13.96	0.00
Y-Seismic+%5	-10.15	-4.36	1.75	0.00	0.38	-0.87	0.13
Y-Seismic-%5	-12.39	-5.43	-0.61	0.00	0.40	-2.02	0.13
X-Wind +%5	-0.62	1.25	2.96	0.00	0.00	1.40	0.00
X-Wind -%5	-0.45	1.33	3.13	0.00	0.00	1.49	0.00
Y-Wind +%5	-1.43	-0.63	0.24	0.00	0.05	-0.13	0.02
Y-Wind -%5	-1.75	-0.78	-0.09	0.00	0.06	-0.29	0.02



Material: E1 C25 S420 (t,m)

DESIGN : X-(G+Q) X-(G+Q+E) Y-(G+Q) Y-(G+Q+E) Y-(Soil)

max. Nd (t) : 49.824 39.153 49.824 47.328 49.824

max. M (tm) : -1.331 29.523 1.246 1.183 0.924

fcd (kg/cm²) : 166.667 166.667 166.667 166.667 166.667

μ : 0.0010 0.0010 0.0013 0.0013 0.001

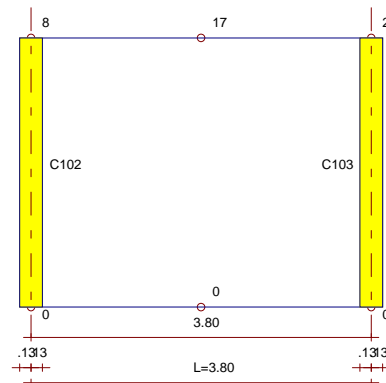
As (cm²) : 7.065 7.065 8.831 8.831 3.125

REINF : 2x13ø12 (vertical) + ø8/15 (vertical)

PB14 PANEL

I/K:8/0 Io/Jo:17/0 J/L:25/ Bx/By :355./25. Hk :3.0 m Cqa=1.000

COMBINATION	maxNd	upMx	dwMx	upMy	dwMy	Tx	Ty
1. (G+G+G+G)	37.15	-2.32	0.79	0.00	0.00	-0.51	0.00
2. (Q+Q+Q+Q)	6.36	-0.67	0.23	0.00	0.00	-0.15	0.00
3. (o+Q+o+Q)	3.36	-0.40	0.08	0.00	0.00	-0.10	0.00
4. (Q+o+Q+o)	2.93	-0.28	0.14	0.00	0.00	-0.05	0.00
5. (Q+Q+o+Q)	4.53	-0.33	0.16	0.00	0.00	-0.06	0.00
6. (o+Q+Q+o)	4.13	-0.44	0.08	0.00	0.00	-0.12	0.00
7. (o+o+Q+Q)	3.92	-0.58	0.21	0.00	0.00	-0.13	0.00
Soil	-0.01	-0.53	-0.99	0.00	-0.01	-0.51	0.00
X-Seismic+%5	0.72	20.67	37.78	0.00	0.01	19.48	0.00
X-Seismic-%5	2.39	22.46	39.94	0.00	-0.01	20.80	0.00
Y-Seismic+%5	-6.80	0.45	1.49	0.00	0.48	0.65	0.16
Y-Seismic-%5	-9.27	-2.08	-1.53	0.00	0.49	-1.20	0.16
X-Wind +%5	0.08	2.21	4.04	0.00	0.00	2.08	0.00
X-Wind -%5	0.26	2.40	4.26	0.00	0.00	2.22	0.00
Y-Wind +%5	-0.95	0.06	0.20	0.00	0.07	0.09	0.02
Y-Wind -%5	-1.30	-0.30	-0.22	0.00	0.07	-0.17	0.02



Material: E1 C25 S420 (t,m)

DESIGN : X-(G+Q) X-(G+Q+E) Y-(G+Q) Y-(G+Q+E) Y-(Soil)

max. Nd (t) : 62.174 45.897 62.174 52.775 62.174

max. M (tm) : -5.173 40.964 1.554 1.319 0.924

fcd (kg/cm²) : 166.667 166.667 166.667 166.667 166.667

μ : 0.0010 0.0010 0.0013 0.0013 0.001

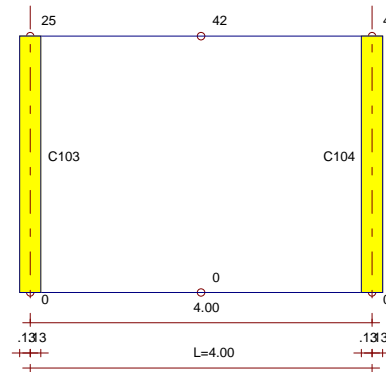
As (cm²) : 8.875 8.875 11.094 11.094 3.125

REINF : 2x16ø12 (vertical) + ø8/15 (vertical)

PB15 PANEL

I/K:25/0 Io/Jo:42/0 J/L:43/ Bx/By :375./25. Hk :3.0 m Cqa=1.000

COMBINATION	maxNd	upMx	dwMx	upMy	dwMy	Tx	Ty
1. (G+G+G+G)	40.65	-0.82	0.38	0.00	0.00	-0.15	0.00
2. (Q+Q+Q+Q)	7.19	-0.20	0.10	0.00	0.00	-0.03	0.00
3. (o+Q+o+Q)	3.99	-0.11	0.00	0.00	0.00	-0.04	0.00
4. (Q+o+Q+o)	3.14	-0.09	0.09	0.00	0.00	0.00	0.00
5. (Q+Q+o+Q)	5.01	-0.28	0.16	0.00	0.00	-0.04	0.00
6. (o+Q+Q+o)	4.51	-0.01	-0.05	0.00	0.00	-0.02	0.00
7. (o+o+Q+Q)	4.72	-0.11	0.07	0.00	0.00	-0.01	0.00
Soil	0.00	-0.57	-1.07	0.00	-0.02	-0.55	-0.01
X-Seismic+%5	0.22	22.02	40.83	0.00	0.00	20.95	0.00
X-Seismic-%5	0.88	23.99	43.12	0.00	0.00	22.37	0.00
Y-Seismic+%5	-7.43	1.08	1.42	0.00	0.51	0.83	0.17
Y-Seismic-%5	-8.40	-1.73	-1.78	0.00	0.51	-1.17	0.17
X-Wind +%5	0.02	2.35	4.36	0.00	0.00	2.24	0.00
X-Wind -%5	0.09	2.56	4.60	0.00	0.00	2.39	0.00
Y-Wind +%5	-1.04	0.15	0.19	0.00	0.07	0.11	0.02
Y-Wind -%5	-1.18	-0.24	-0.26	0.00	0.07	-0.17	0.02



Material: E1 C25 S420 (t,m)

DESIGN : X-(G+Q) X-(G+Q+E) Y-(G+Q) Y-(G+Q+E) Y-(Soil)

max. Nd (t) : 68.417 48.719 68.417 56.239 68.417

max. M (tm) : -2.524 43.671 1.710 1.406 0.924

fcd (kg/cm²) : 166.667 166.667 166.667 166.667 166.667

μ : 0.0010 0.0010 0.0013 0.0013 0.001

As (cm²) : 9.375 9.375 11.719 11.719 3.125

REINF : 2x17ø12 (vertical) + ø8/15 (vertical)

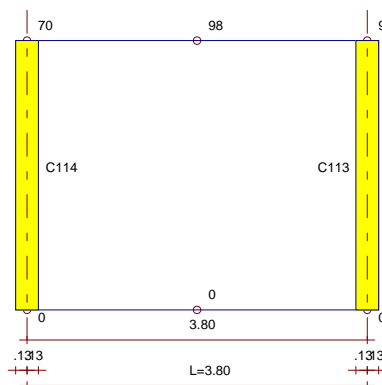
PROJECT :DENE ME

(DENE .ST4)

PB29 PANEL

I/K:70/0 Io/Jo:98/0 J/L:97/ Bx/By :355./25. Hk :3.0 m Cqa=1.000

COMBINATION	maxNd	upMx	dwMx	upMy	dwMy	Tx	Ty
1. (G+G+G+G)	37.31	2.55	-0.66	0.00	0.00	0.63	0.00
2. (Q+Q+Q+Q)	6.41	0.75	-0.20	0.00	0.00	0.18	0.00
3. (o+Q+o+Q)	3.66	0.24	-0.10	0.00	0.00	0.04	0.00
4. (Q+o+Q+o)	2.69	0.50	-0.09	0.00	0.00	0.14	0.00
5. (Q+Q+o+Q)	4.71	0.58	-0.11	0.00	0.00	0.16	0.00
6. (o+Q+Q+o)	4.24	0.43	-0.18	0.00	0.00	0.08	0.00
7. (o+o+Q+Q)	3.75	0.48	-0.11	0.00	0.00	0.12	0.00
Soil	0.01	-0.57	-0.98	0.00	-0.01	-0.52	0.00
X-Seismic+%5	-0.89	20.64	37.79	0.00	-0.01	19.48	0.00
X-Seismic-%5	-2.31	22.45	39.94	0.00	0.01	20.80	0.00
Y-Seismic+%5	-8.10	1.65	1.13	0.00	0.50	0.92	0.17
Y-Seismic-%5	-6.01	-0.93	-1.87	0.00	0.47	-0.93	0.16
X-Wind +%5	-0.10	2.21	4.04	0.00	0.00	2.08	0.00
X-Wind -%5	-0.25	2.40	4.26	0.00	0.00	2.22	0.00
Y-Wind +%5	-1.14	0.23	0.15	0.00	0.07	0.13	0.02
Y-Wind -%5	-0.85	-0.13	-0.27	0.00	0.07	-0.13	0.02



Material: E1 C25 S420 (t,m)

DESIGN : X-(G+Q) X-(G+Q+E) Y-(G+Q) Y-(G+Q+E) Y-(Soil)

max. Nd (t) : 62.513 46.048 62.513 51.834 62.513

max. M (tm) : 4.756 39.283 1.563 1.296 0.924

fcd (kg/cm²) : 166.667 166.667 166.667 166.667 166.667

μ : 0.0010 0.0010 0.0013 0.0013 0.001

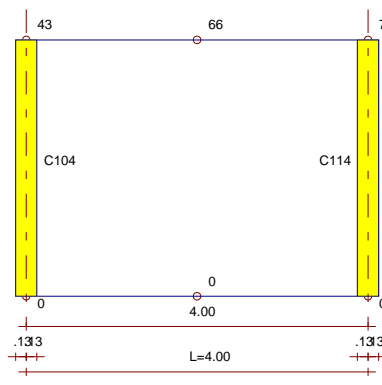
As (cm²) : 8.875 8.875 11.094 11.094 3.125

REINF : 2x16ø12 (vertical) + ø8/15 (vertical)

PB30 PANEL

I/K:43/0 Io/Jo:66/0 J/L:70/ Bx/By :375./25. Hk :3.0 m Cqa=1.000

COMBINATION	maxNd	upMx	dwMx	upMy	dwMy	Tx	Ty
1. (G+G+G+G)	40.81	0.76	-0.15	0.00	0.00	0.21	0.00
2. (Q+Q+Q+Q)	7.25	0.17	-0.03	0.00	0.00	0.05	0.00
3. (o+Q+o+Q)	3.79	0.05	-0.05	0.00	0.00	0.00	0.00
4. (Q+o+Q+o)	3.39	0.12	0.02	0.00	0.00	0.05	0.00
5. (Q+Q+o+Q)	5.39	0.12	0.03	0.00	0.00	0.05	0.00
6. (o+Q+Q+o)	4.42	-0.10	-0.02	0.00	0.00	-0.04	0.00
7. (o+o+Q+Q)	4.57	0.30	-0.07	0.00	0.00	0.08	0.00
Soil	0.01	-0.57	-1.07	0.00	-0.02	-0.55	-0.01
X-Seismic+%5	-0.34	22.11	40.80	0.00	0.00	20.97	0.00
X-Seismic-%5	-0.73	24.06	43.10	0.00	0.00	22.39	0.00
Y-Seismic+%5	-7.80	0.99	1.45	0.00	0.52	0.81	0.17
Y-Seismic-%5	-7.22	-1.79	-1.76	0.00	0.51	-1.18	0.17
X-Wind +%5	-0.04	2.36	4.36	0.00	0.00	2.24	0.00
X-Wind -%5	-0.08	2.57	4.59	0.00	0.00	2.39	0.00
Y-Wind +%5	-1.09	0.14	0.19	0.00	0.07	0.11	0.02
Y-Wind -%5	-1.01	-0.25	-0.25	0.00	0.07	-0.17	0.02



Material: E1 C25 S420 (t,m)

DESIGN : X-(G+Q) X-(G+Q+E) Y-(G+Q) Y-(G+Q+E) Y-(Soil)

max. Nd (t) : 68.740 48.796 68.740 55.867 68.740

max. M (tm) : -2.021 42.980 1.718 1.397 0.924

fcd (kg/cm²) : 166.667 166.667 166.667 166.667 166.667

μ : 0.0010 0.0010 0.0013 0.0013 0.001

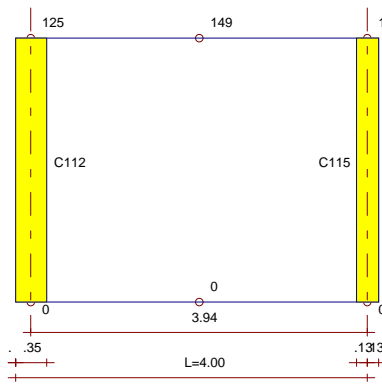
As (cm²) : 9.375 9.375 11.719 11.719 3.125

REINF : 2x17ø12 (vertical) + ø8/15 (vertical)

PB31 PANEL

I/K:125/0 Io/Jo:149/0 J/L:127/ Bx/By :25./352.6 Hk :3.0 m Cqa=1.000

COMBINATION	maxNd	upMx	dwMx	upMy	dwMy	Tx	Ty
1. (G+G+G+G)	31.64	0.00	0.00	-0.34	0.11	0.00	-0.08
2. (Q+Q+Q+Q)	4.46	0.00	0.00	-0.77	0.24	0.00	-0.18
3. (o+Q+o+Q)	2.50	0.00	0.00	-0.26	0.18	0.00	-0.03
4. (Q+o+Q+o)	1.91	0.00	0.00	-0.51	0.06	0.00	-0.15
5. (Q+Q+o+Q)	3.31	0.00	0.00	-0.44	0.03	0.00	-0.13
6. (o+Q+Q+o)	2.80	0.00	0.00	-0.61	0.14	0.00	-0.16
7. (o+o+Q+Q)	2.71	0.00	0.00	-0.49	0.30	0.00	-0.06
Soil	0.04	0.00	-0.01	-0.94	-1.84	0.00	-0.93
X-Seismic+%5	9.94	0.00	0.31	2.51	-3.00	0.10	-0.16
X-Seismic-%5	10.56	0.00	0.33	3.17	1.23	0.11	1.46
Y-Seismic+%5	-4.82	0.00	0.01	23.19	66.30	0.00	29.83
Y-Seismic-%5	-5.75	0.00	-0.01	22.34	60.32	0.00	27.55
X-Wind +%5	1.07	0.00	0.03	0.27	-0.32	0.01	-0.02
X-Wind -%5	1.14	0.00	0.03	0.33	0.13	0.01	0.15
Y-Wind +%5	-0.68	0.00	0.00	3.33	9.49	0.00	4.27
Y-Wind -%5	-0.82	0.00	0.00	3.21	8.64	0.00	3.95



Material: E1 C25 S420 (t,m)

DESIGN : X-(G+Q) X-(G+Q+E) Y-(G+Q) Y-(G+Q+E) X-(Soil)

max. Nd (t) : 51.502 46.709 51.502 40.967 51.502

max. M (tm) : 1.288 1.168 -3.222 66.703 -1.108

fcd (kg/cm²) : 166.667 166.667 166.667 166.667 166.667

μ : 0.0013 0.0013 0.0010 0.0010 0.001

As (cm²) : 11.019 11.019 8.815 8.815 3.125

REINF : 2x16ø12 (vertical) + ø8/15 (vertical)

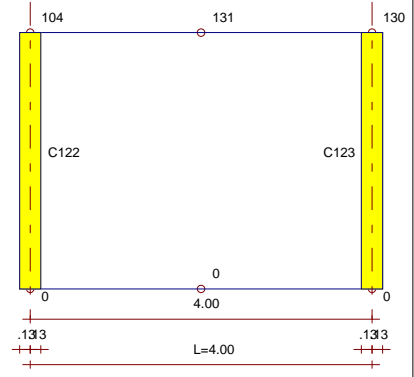
PROJECT : DENE ME

(DENE . ST4)

PB44 PANEL

I/K:104/0 Io/Jo:131/0 J/L:130/ Bx/By :375./25. Hk :3.0 m Cqa=1.000

COMBINATION	maxNd	upMx	dwMx	upMy	dwMy	Tx	Ty
1. (G+G+G+G)	40.65	-0.82	0.38	0.00	0.00	-0.15	0.00
2. (Q+Q+Q+Q)	7.19	-0.20	0.10	0.00	0.00	-0.03	0.00
3. (o+Q+o+Q)	3.67	-0.39	0.08	0.00	0.00	-0.11	0.00
4. (Q+o+Q+o)	3.46	0.19	0.02	0.00	0.00	0.07	0.00
5. (Q+Q+o+Q)	5.06	-0.27	0.18	0.00	0.00	-0.03	0.00
6. (o+Q+Q+o)	4.48	0.00	-0.05	0.00	0.00	-0.02	0.00
7. (o+o+Q+Q)	4.72	-0.13	0.06	0.00	0.00	-0.02	0.00
Soil	-0.01	-0.58	-1.08	0.00	-0.02	-0.55	-0.01
X-Seismic+%5	0.88	23.99	43.12	0.00	0.00	22.37	0.00
X-Seismic-%5	0.22	22.02	40.83	0.00	0.00	20.95	0.00
Y-Seismic+%5	7.43	-1.08	-1.42	0.00	0.51	-0.83	0.17
Y-Seismic-%5	8.40	1.73	1.78	0.00	0.51	1.17	0.17
X-Wind +%5	0.09	2.56	4.60	0.00	0.00	2.39	0.00
X-Wind -%5	0.02	2.35	4.36	0.00	0.00	2.24	0.00
Y-Wind +%5	1.04	-0.15	-0.19	0.00	0.07	-0.11	0.02
Y-Wind -%5	1.18	0.24	0.26	0.00	0.07	0.17	0.02



Material: E1 C25 S420 (t,m)

DESIGN : X-(G+Q) X-(G+Q+E) Y-(G+Q) Y-(G+Q+E) Y-(Soil)

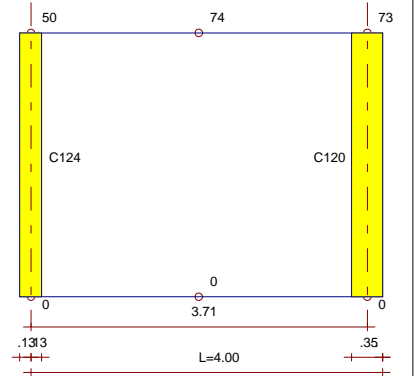
max. Nd (t) :	68.421	48.721	68.421	56.241	68.421
max. M (tm) :	-2.702	43.685	1.711	1.406	-1.108
fcd (kg/cm ²) :	166.667	166.667	166.667	166.667	166.667
μ :	0.0010	0.0010	0.0013	0.0013	0.001
As (cm ²) :	9.375	9.375	11.719	11.719	3.125

REINF : 2x17ø12 (vertical) + ø8/15 (vertical)

PB45 PANEL

I/K:50/0 Io/Jo:74/0 J/L:73/ Bx/By :25./352.6 Hk :3.0 m Cqa=1.000

COMBINATION	maxNd	upMx	dwMx	upMy	dwMy	Tx	Ty
1. (G+G+G+G)	31.46	0.00	0.00	0.28	-0.09	0.00	0.06
2. (Q+Q+Q+Q)	4.41	0.00	0.00	0.75	-0.24	0.00	0.17
3. (o+Q+o+Q)	2.17	0.00	0.00	0.53	-0.09	0.00	0.15
4. (Q+o+Q+o)	2.19	0.00	0.00	0.21	-0.14	0.00	0.02
5. (Q+Q+o+Q)	3.33	0.00	0.00	0.35	-0.19	0.00	0.05
6. (o+Q+Q+o)	2.55	0.00	0.00	0.38	-0.16	0.00	0.07
7. (o+o+Q+Q)	2.84	0.00	0.00	0.76	-0.12	0.00	0.21
Soil	-0.04	0.00	-0.01	-0.95	-1.86	0.00	-0.94
X-Seismic+%5	-10.58	0.00	0.33	2.82	0.74	0.11	1.19
X-Seismic-%5	-9.94	0.00	0.31	2.82	-2.50	0.10	0.11
Y-Seismic+%5	5.35	0.00	-0.01	22.33	61.94	0.00	28.09
Y-Seismic-%5	4.41	0.00	0.01	22.20	66.48	0.00	29.56
X-Wind +%5	-1.14	0.00	0.03	0.29	0.07	0.01	0.12
X-Wind -%5	-1.07	0.00	0.03	0.31	-0.26	0.01	0.02
Y-Wind +%5	0.76	0.00	0.00	3.23	8.90	0.00	4.04
Y-Wind -%5	0.62	0.00	0.00	3.20	9.52	0.00	4.24



Material: E1 C25 S420 (t,m)

DESIGN : X-(G+Q) X-(G+Q+E) Y-(G+Q) Y-(G+Q+E) X-(Soil)

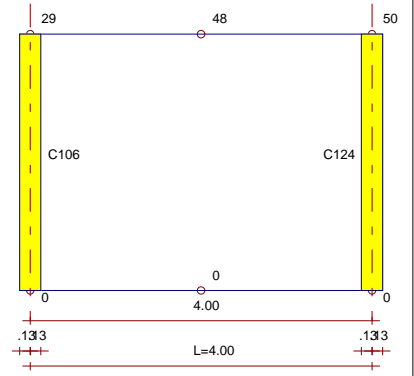
max. Nd (t) :	51.102	46.451	51.102	40.281	51.102
max. M (tm) :	1.278	1.161	-3.472	66.390	0.924
fcd (kg/cm ²) :	166.667	166.667	166.667	166.667	166.667
μ :	0.0013	0.0013	0.0010	0.0010	0.001
As (cm ²) :	11.019	11.019	8.815	8.815	3.125

REINF : 2x16ø12 (vertical) + ø8/15 (vertical)

PB46 PANEL

I/K:29/0 Io/Jo:48/0 J/L:50/ Bx/By :25./375. Hk :3.0 m Cqa=1.000

COMBINATION	maxNd	upMx	dwMx	upMy	dwMy	Tx	Ty
1. (G+G+G+G)	36.73	0.00	0.00	1.26	-0.42	0.00	0.28
2. (Q+Q+Q+Q)	5.89	0.00	0.00	0.34	-0.11	0.00	0.08
3. (o+Q+o+Q)	3.22	0.00	0.00	0.22	0.01	0.00	0.08
4. (Q+o+Q+o)	2.60	0.00	0.00	0.11	-0.12	0.00	0.00
5. (Q+Q+o+Q)	3.96	0.00	0.00	0.03	-0.09	0.00	-0.02
6. (o+Q+Q+o)	3.73	0.00	0.00	0.38	-0.17	0.00	0.07
7. (o+o+Q+Q)	3.97	0.00	0.00	0.27	0.04	0.00	0.10
Soil	0.01	0.00	-0.01	-1.03	-1.93	0.00	-0.99
X-Seismic+%5	-10.42	0.00	0.34	0.97	1.39	0.11	0.79
X-Seismic-%5	-9.52	0.00	0.34	-1.46	-1.23	0.11	-0.89
Y-Seismic+%5	-0.89	0.00	0.00	33.10	61.84	0.00	31.65
Y-Seismic-%5	-2.22	0.00	0.00	36.54	65.45	0.00	34.00
X-Wind +%5	-1.13	0.00	0.04	0.10	0.14	0.01	0.08
X-Wind -%5	-1.03	0.00	0.04	-0.15	-0.12	0.01	-0.09
Y-Wind +%5	-0.12	0.00	0.00	4.75	8.89	0.00	4.55
Y-Wind -%5	-0.31	0.00	0.00	5.23	9.38	0.00	4.87



Material: E1 C25 S420 (t,m)

DESIGN : X-(G+Q) X-(G+Q+E) Y-(G+Q) Y-(G+Q+E) X-(Soil)

max. Nd (t) :	60.865	53.050	60.865	44.849	60.865
max. M (tm) :	1.522	1.326	-3.960	65.060	0.924
fcd (kg/cm ²) :	166.667	166.667	166.667	166.667	166.667
μ :	0.0013	0.0013	0.0010	0.0010	0.001
As (cm ²) :	11.719	11.719	9.375	9.375	3.125

REINF : 2x17ø12 (vertical) + ø8/15 (vertical)

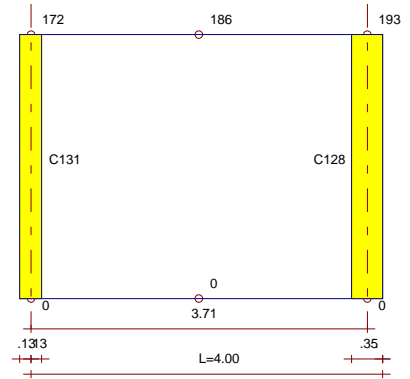
PROJECT :DENEEME

(DENE.ST4)

PB57 PANEL

I/K:172/0 Io/Jo:186/0 J/L:193/ Bx/By :25./352.6 Hk :3.0 m Cqa=1.000

COMBINATION	maxNd	upMx	dwMx	upMy	dwMy	Tx	Ty
1.(G+G+G+G)	31.64	0.00	0.00	0.34	-0.11	0.00	0.08
2.(Q+Q+Q+Q)	4.46	0.00	0.00	0.77	-0.24	0.00	0.18
3.(o+Q+o+Q)	2.17	0.00	0.00	0.53	-0.06	0.00	0.16
4.(Q+o+Q+o)	2.23	0.00	0.00	0.23	-0.18	0.00	0.02
5.(Q+Q+o+Q)	3.36	0.00	0.00	0.35	-0.21	0.00	0.05
6.(o+Q+Q+o)	2.58	0.00	0.00	0.40	-0.17	0.00	0.08
7.(o+o+Q+Q)	2.87	0.00	0.00	0.78	-0.09	0.00	0.23
Soil	-0.17	0.00	-0.01	-0.75	-1.90	0.00	-0.88
X-Seismic+%5	10.56	0.00	0.33	-3.17	-1.23	0.11	-1.46
X-Seismic-%5	9.94	0.00	0.31	-2.51	3.00	0.10	0.16
Y-Seismic+%5	4.82	0.00	-0.01	23.19	66.30	0.00	29.83
Y-Seismic-%5	5.75	0.00	0.01	22.34	60.32	0.00	27.55
X-Wind +%5	1.14	0.00	0.03	-0.33	-0.13	0.01	-0.15
X-Wind -%5	1.07	0.00	0.03	-0.27	0.32	0.01	0.02
Y-Wind +%5	0.68	0.00	0.00	3.33	9.49	0.00	4.27
Y-Wind -%5	0.82	0.00	0.00	3.21	8.64	0.00	3.95

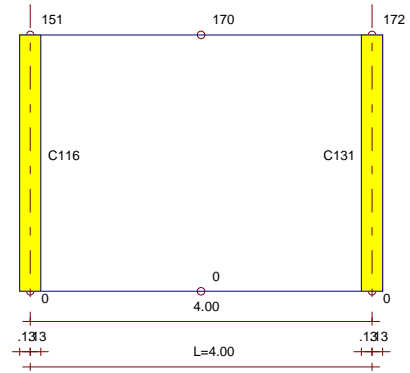


Material:E1 C25 S420 (t,m)
DESIGN : X-(G+Q) X-(G+Q+E) Y-(G+Q) Y-(G+Q+E) X-(Soil)
 max. Nd (t) : 51.436 46.667 51.436 40.925 51.436
 max. M (tm) : 1.286 1.167 -3.575 66.188 -1.108
 fcd (kg/cm²) : 166.667 166.667 166.667 166.667 166.667
 μ : 0.0013 0.0013 0.0010 0.0010 0.0010
 As (cm²) : 11.019 11.019 8.815 8.815 3.125
REINF :2x16ø12 (vertical) + ø8/15 (vertical)

PB58 PANEL

I/K:151/0 Io/Jo:170/0 J/L:172/ Bx/By :25./375. Hk :3.0 m Cqa=1.000

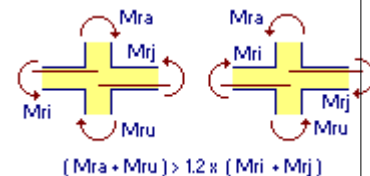
COMBINATION	maxNd	upMx	dwMx	upMy	dwMy	Tx	Ty
1.(G+G+G+G)	37.09	0.00	0.00	1.37	-0.46	0.00	0.30
2.(Q+Q+Q+Q)	6.01	0.00	0.00	0.38	-0.13	0.00	0.08
3.(o+Q+o+Q)	3.25	0.00	0.00	0.26	0.02	0.00	0.09
4.(Q+o+Q+o)	2.70	0.00	0.00	0.11	-0.15	0.00	-0.01
5.(Q+Q+o+Q)	4.03	0.00	0.00	0.04	-0.12	0.00	-0.03
6.(o+Q+Q+o)	3.81	0.00	0.00	0.40	-0.18	0.00	0.07
7.(o+o+Q+Q)	4.04	0.00	0.00	0.31	0.05	0.00	0.12
Soil	0.01	0.00	-0.01	-1.00	-1.92	0.00	-0.97
X-Seismic+%5	10.33	0.00	0.34	-1.28	-1.92	0.11	-1.07
X-Seismic-%5	9.46	0.00	0.34	1.68	1.78	0.11	1.15
Y-Seismic+%5	-1.71	0.00	0.00	36.08	65.73	0.00	33.94
Y-Seismic-%5	-0.42	0.00	0.00	31.85	60.54	0.00	30.80
X-Wind +%5	1.12	0.00	0.04	-0.14	-0.20	0.01	-0.11
X-Wind -%5	1.03	0.00	0.04	0.18	0.19	0.01	0.12
Y-Wind +%5	-0.24	0.00	0.00	5.17	9.41	0.00	4.86
Y-Wind -%5	-0.06	0.00	0.00	4.57	8.68	0.00	4.42



Material:E1 C25 S420 (t,m)
DESIGN : X-(G+Q) X-(G+Q+E) Y-(G+Q) Y-(G+Q+E) X-(Soil)
 max. Nd (t) : 61.552 53.438 61.552 44.813 61.552
 max. M (tm) : 1.539 1.336 -4.010 65.326 -1.108
 fcd (kg/cm²) : 166.667 166.667 166.667 166.667 166.667
 μ : 0.0013 0.0013 0.0010 0.0010 0.0010
 As (cm²) : 11.719 11.719 9.375 9.375 3.125
REINF :2x17ø12 (vertical) + ø8/15 (vertical)

SHEAR CHECK OF STRONG COLUMNS (t)

Sto	Vsx	Vkx	α_x	Vsy	Vky	α_y
1	151.46	151.46	1.00	154.26	154.26	1.00
2	117.13	128.95	0.91	131.79	137.83	0.96
3	81.86	114.97	0.71	114.66	122.98	0.93
4	90.03	90.03	1.00	97.28	97.28	1.00
5	54.82	54.82	1.00	60.54	60.54	1.00
6	3.75	3.75	1.00	4.92	4.92	1.00



Vs/Vk > .70 CONDITION IS SATISFIED STRONG COLUMNS NOT MULTIPLIED BY (1/α)

STRONG COLUMN CHECK (tm)

Dir	Column	Mrc	Beam	Mrb	EXPLANATION
+X	C501 (3.74)	3.74	B513 (6.35)	7.62	Bldg. upper level cnd.
-X	C501 (3.74)	3.74	B513 (7.08)	8.5	Bldg. upper level cnd.
+Y	C501 (5.57)	5.57	B516 (4.29)	5.14	Bldg. upper level cnd.
-Y	C501 (5.57)	5.57	B516 (8.35)	10.02	Bldg. upper level cnd.
+X	C501 (3.74)+C401 (4.32)	8.06	B413 (6.35)	7.62	Nd < 0,10.Ac.fck conditio
-X	C501 (3.74)+C401 (4.32)	8.06	B413 (7.08)	8.5	Nd < 0,10.Ac.fck conditio
+Y	C501 (5.57)+C401 (6.4)	11.97	B416 (4.29)	5.14	Nd < 0,10.Ac.fck conditio
-Y	C501 (5.57)+C401 (6.4)	11.97	B416 (8.35)	10.02	Nd < 0,10.Ac.fck conditio
+X	C401 (4.32)+C301 (4.89)	9.21	B313 (6.35)	7.62	Nd < 0,10.Ac.fck conditio
-X	C401 (4.32)+C301 (4.89)	9.21	B313 (7.08)	8.5	Nd < 0,10.Ac.fck conditio
+Y	C401 (6.4)+C301 (7.13)	13.53	B316 (6.35)	7.62	Nd < 0,10.Ac.fck conditio
-Y	C401 (6.4)+C301 (7.13)	13.53	B316 (8.35)	10.02	Nd < 0,10.Ac.fck conditio
+X	C301 (4.89)+CZ01 (5.38)	10.26	BZ13 (6.35)	7.62	✓
-X	C301 (4.89)+CZ01 (5.38)	10.26	BZ13 (7.08)	8.5	✓
+Y	C301 (7.13)+CZ01 (7.49)	14.62	BZ16 (6.35)	7.62	✓
-Y	C301 (7.13)+CZ01 (7.49)	14.62	BZ16 (8.35)	10.02	✓
+X	CZ01 (5.38)+CB01 (3.88)	9.25	BB13 (6.35)	7.62	Panel end zone
-X	CZ01 (5.38)+CB01 (3.88)	9.25	BB13 (7.08)	8.5	Panel end zone
+Y	CZ01 (7.49)+CB01 (5.82)	13.31	BB16 (6.35)	7.62	Panel end zone
-Y	CZ01 (7.49)+CB01 (5.82)	13.31	BB16 (8.35)	10.02	Panel end zone
+X	C502 (3.95)	3.95	B513 (8.35)+B514 (4.29)	15.17	Bldg. upper level cnd.
-X	C502 (3.95)	3.95	B513 (6.35)+B514 (8.35)	17.65	Bldg. upper level cnd.
+Y	C502 (5.99)	5.99	B509 (4.29)	5.14	Bldg. upper level cnd.
-Y	C502 (5.99)	5.99	B509 (8.35)	10.02	Bldg. upper level cnd.
+X	C502 (3.95)+C402 (4.6)	8.55	B413 (8.35)+B414 (4.29)	15.17	Nd < 0,10.Ac.fck conditio
-X	C502 (3.95)+C402 (4.6)	8.55	B413 (6.35)+B414 (8.35)	17.65	Nd < 0,10.Ac.fck conditio
+Y	C502 (5.99)+C402 (7.13)	13.11	B409 (4.29)	5.14	Nd < 0,10.Ac.fck conditio
-Y	C502 (5.99)+C402 (7.13)	13.11	B409 (8.35)	10.02	Nd < 0,10.Ac.fck conditio
+X	C402 (4.6)+C302 (5.17)	9.76	B313 (8.35)+B314 (4.29)	15.17	INSUFFICIENT!
-X	C402 (4.6)+C302 (5.17)	9.76	B313 (6.35)+B314 (8.35)	17.65	INSUFFICIENT!
+Y	C402 (7.13)+C302 (7.69)	14.82	B309 (6.35)	7.62	✓
-Y	C402 (7.13)+C302 (7.69)	14.82	B309 (9.06)	10.88	✓
+X	C302 (5.17)+CZ02 (6.04)	11.21	BZ13 (8.35)+BZ14 (4.29)	15.17	INSUFFICIENT!
-X	C302 (5.17)+CZ02 (6.04)	11.21	BZ13 (6.35)+BZ14 (8.35)	17.65	INSUFFICIENT!
+Y	C302 (7.69)+CZ02 (8.11)	15.8	BZ09 (6.35)	7.62	✓
-Y	C302 (7.69)+CZ02 (8.11)	15.8	BZ09 (9.06)	10.88	✓
+X	CZ02 (6.04)+CB02 (3.73)	9.77	BB13 (8.35)+BB14 (4.29)	15.17	Panel end zone
-X	CZ02 (6.04)+CB02 (3.73)	9.77	BB13 (6.35)+BB14 (8.35)	17.65	Panel end zone
+Y	CZ02 (8.11)+CB02 (5.69)	13.8	BB09 (4.29)	5.14	Panel end zone
-Y	CZ02 (8.11)+CB02 (5.69)	13.8	BB09 (8.35)	10.02	Panel end zone
+X	C503 (4.08)	4.08	B514 (8.35)+B515 (4.29)	15.17	Bldg. upper level cnd.
-X	C503 (4.08)	4.08	B514 (4.29)+B515 (8.35)	15.17	Bldg. upper level cnd.
+Y	C503 (6.13)	6.13	B511 (4.29)	5.14	Bldg. upper level cnd.
-Y	C503 (6.13)	6.13	B511 (8.35)	10.02	Bldg. upper level cnd.
+X	C503 (4.08)+C403 (4.88)	8.96	B414 (8.35)+B415 (4.29)	15.17	Nd < 0,10.Ac.fck conditio
-X	C503 (4.08)+C403 (4.88)	8.96	B414 (4.29)+B415 (8.35)	15.17	Nd < 0,10.Ac.fck conditio
+Y	C503 (6.13)+C403 (7.3)	13.43	B411 (4.29)	5.14	✓
-Y	C503 (6.13)+C403 (7.3)	13.43	B411 (8.35)	10.02	✓
+X	C403 (4.88)+C303 (5.6)	10.47	B314 (8.35)+B315 (4.29)	15.17	INSUFFICIENT!
-X	C403 (4.88)+C303 (5.6)	10.47	B314 (4.29)+B315 (8.35)	15.17	INSUFFICIENT!
+Y	C403 (7.3)+C303 (7.81)	15.12	B311 (6.35)	7.62	✓
-Y	C403 (7.3)+C303 (7.81)	15.12	B311 (8.35)	10.02	✓
+X	C303 (5.6)+CZ03 (6.18)	11.77	BZ14 (8.35)+BZ15 (4.29)	15.17	INSUFFICIENT!
-X	C303 (5.6)+CZ03 (6.18)	11.77	BZ14 (4.29)+BZ15 (8.35)	15.17	INSUFFICIENT!
+Y	C303 (7.81)+CZ03 (8.21)	16.03	BZ11 (6.35)	7.62	✓
-Y	C303 (7.81)+CZ03 (8.21)	16.03	BZ11 (8.35)	10.02	✓

STRONG COLUMN CHECK (tm)

Dir	Column	Mrc	Beam	Mrb	EXPLANATION
+X	C507 (8.52)+C407 (9.6)	18.11	B401 (8.35)+B402 (4.29)	15.18	Nd < 0,10.Ac.fck conditio
-X	C507 (8.52)+C407 (9.6)	18.11	B401 (6.35)+B402 (8.35)	17.65	Nd < 0,10.Ac.fck conditio
+Y	C507 (8.51)+C407 (9.64)	18.15	B409 (8.35)+B410 (4.29)	15.17	Nd < 0,10.Ac.fck conditio
-Y	C507 (8.51)+C407 (9.64)	18.15	B409 (4.29)+B410 (8.35)	15.17	Nd < 0,10.Ac.fck conditio
+X	C407 (9.6)+C307 (10.38)	19.98	B301 (8.35)+B302 (4.29)	15.18	✓
-X	C407 (9.6)+C307 (10.38)	19.98	B301 (6.35)+B302 (8.35)	17.65	✓
+Y	C407 (9.64)+C307 (10.45)	20.09	B309 (10.3)+B310 (6.35)	19.98	✓
-Y	C407 (9.64)+C307 (10.45)	20.09	B309 (6.35)+B310 (10.3)	19.98	✓
+X	C307 (10.38)+CZ07 (10.88)	21.26	BZ01 (8.35)+BZ02 (4.29)	15.18	✓
-X	C307 (10.38)+CZ07 (10.88)	21.26	BZ01 (6.35)+BZ02 (8.35)	17.65	✓
+Y	C307 (10.45)+CZ07 (10.93)	21.39	BZ09 (8.35)+BZ10 (6.35)	17.64	✓
-Y	C307 (10.45)+CZ07 (10.93)	21.39	BZ09 (6.35)+BZ10 (8.35)	17.64	✓
+X	CZ07 (10.88)+CB07 (11.45)	22.33	BB01 (8.35)+BB02 (4.29)	15.18	Basement
-X	CZ07 (10.88)+CB07 (11.45)	22.33	BB01 (6.35)+BB02 (8.35)	17.65	Basement
+Y	CZ07 (10.93)+CB07 (11.4)	22.33	BB09 (8.35)+BB10 (4.29)	15.17	Basement
-Y	CZ07 (10.93)+CB07 (11.4)	22.33	BB09 (4.29)+BB10 (8.35)	15.17	Basement
+X	C508 (8.61)	8.61	B502 (8.35)+B503 (4.29)	15.18	Bldg. upper level cnd.
-X	C508 (8.61)	8.61	B502 (4.29)+B503 (8.35)	15.18	Bldg. upper level cnd.
+Y	C508 (8.64)	8.64	B511 (8.35)+B512 (4.29)	15.17	Bldg. upper level cnd.
-Y	C508 (8.64)	8.64	B511 (4.29)+B512 (8.35)	15.17	Bldg. upper level cnd.
+X	C508 (8.61)+C408 (9.8)	18.41	B402 (8.35)+B403 (4.29)	15.18	Nd < 0,10.Ac.fck conditio
-X	C508 (8.61)+C408 (9.8)	18.41	B402 (4.29)+B403 (8.35)	15.18	Nd < 0,10.Ac.fck conditio
+Y	C508 (8.64)+C408 (9.85)	18.49	B411 (8.35)+B412 (4.29)	15.17	Nd < 0,10.Ac.fck conditio
-Y	C508 (8.64)+C408 (9.85)	18.49	B411 (4.29)+B412 (8.35)	15.17	Nd < 0,10.Ac.fck conditio
+X	C408 (9.8)+C308 (10.6)	20.41	B302 (8.35)+B303 (4.29)	15.18	✓
-X	C408 (9.8)+C308 (10.6)	20.41	B302 (4.29)+B303 (8.35)	15.18	✓
+Y	C408 (9.85)+C308 (10.63)	20.48	B311 (8.35)+B312 (4.29)	15.17	✓
-Y	C408 (9.85)+C308 (10.63)	20.48	B311 (4.29)+B312 (8.35)	15.17	✓
+X	C308 (10.6)+CZ08 (11.17)	21.77	BZ02 (8.35)+BZ03 (4.29)	15.18	✓
-X	C308 (10.6)+CZ08 (11.17)	21.77	BZ02 (4.29)+BZ03 (8.35)	15.18	✓
+Y	C308 (10.63)+CZ08 (11.19)	21.82	BZ11 (8.35)+BZ12 (4.29)	15.17	✓
-Y	C308 (10.63)+CZ08 (11.19)	21.82	BZ11 (4.29)+BZ12 (8.35)	15.17	✓
+X	CZ08 (11.17)+CB08 (11.61)	22.78	BB02 (8.35)+BB03 (4.29)	15.18	Basement
-X	CZ08 (11.17)+CB08 (11.61)	22.78	BB02 (4.29)+BB03 (8.35)	15.18	Basement
+Y	CZ08 (11.19)+CB08 (11.6)	22.79	BB11 (8.35)+BB12 (4.29)	15.17	Basement
-Y	CZ08 (11.19)+CB08 (11.6)	22.79	BB11 (4.29)+BB12 (8.35)	15.17	Basement
+X	C509 (8.39)	8.39	B503 (8.35)+B520 (4.29)	15.18	Bldg. upper level cnd.
-X	C509 (8.39)	8.39	B503 (4.29)+B520 (8.35)	15.18	Bldg. upper level cnd.
+Y	C509 (8.19)	8.19	B506 (8.35)+B507 (6.35)	17.64	Bldg. upper level cnd.
-Y	C509 (8.19)	8.19	B506 (4.29)+B507 (8.35)	15.17	Bldg. upper level cnd.
+X	C509 (8.39)+C409 (9.47)	17.86	B403 (8.35)+B420 (4.29)	15.18	Nd < 0,10.Ac.fck conditio
-X	C509 (8.39)+C409 (9.47)	17.86	B403 (4.29)+B420 (8.35)	15.18	Nd < 0,10.Ac.fck conditio
+Y	C509 (8.19)+C409 (9.15)	17.34	B406 (8.35)+B407 (8.35)	20.05	Nd < 0,10.Ac.fck conditio
-Y	C509 (8.19)+C409 (9.15)	17.34	B406 (6.35)+B407 (8.35)	17.64	Nd < 0,10.Ac.fck conditio
+X	C409 (9.47)+C309 (10.33)	19.79	B303 (10.3)+B320 (6.35)	20	INSUFFICIENT!
-X	C409 (9.47)+C309 (10.33)	19.79	B303 (6.35)+B320 (10.3)	19.99	INSUFFICIENT!
+Y	C409 (9.15)+C309 (9.96)	19.11	B306 (8.35)+B307 (8.35)	20.05	Nd < 0,10.Ac.fck conditio
-Y	C409 (9.15)+C309 (9.96)	19.11	B306 (6.35)+B307 (8.35)	17.64	Nd < 0,10.Ac.fck conditio
+X	C309 (10.33)+CZ09 (10.94)	21.27	BZ03 (8.35)+BZ20 (4.29)	15.18	✓
-X	C309 (10.33)+CZ09 (10.94)	21.27	BZ03 (4.29)+BZ20 (8.35)	15.18	✓
+Y	C309 (9.96)+CZ09 (10.48)	20.44	BZ06 (8.35)+BZ07 (6.35)	17.64	✓
-Y	C309 (9.96)+CZ09 (10.48)	20.44	BZ06 (4.29)+BZ07 (8.35)	15.17	✓
+X	CZ09 (10.94)+CB09 (11.37)	22.31	BB03 (8.35)+BB20 (4.29)	15.18	Basement
-X	CZ09 (10.94)+CB09 (11.37)	22.31	BB03 (4.29)+BB20 (8.35)	15.18	Basement
+Y	CZ09 (10.48)+CB09 (11.32)	21.8	BB06 (8.35)+BB07 (6.35)	17.64	Basement
-Y	CZ09 (10.48)+CB09 (11.32)	21.8	BB06 (4.29)+BB07 (8.35)	15.17	Basement
+X	C510 (8.54)	8.54	B504 (8.35)+B505 (4.29)	15.18	Bldg. upper level cnd.
-X	C510 (8.54)	8.54	B504 (6.35)+B505 (8.35)	17.65	Bldg. upper level cnd.
+Y	C510 (8.53)	8.53	B510 (8.35)+B539 (4.29)	15.17	Bldg. upper level cnd.
-Y	C510 (8.53)	8.53	B510 (4.29)+B539 (8.35)	15.17	Bldg. upper level cnd.
+X	C510 (8.54)+C410 (9.66)	18.2	B404 (8.35)+B405 (4.29)	15.18	Nd < 0,10.Ac.fck conditio
-X	C510 (8.54)+C410 (9.66)	18.2	B404 (6.35)+B405 (8.35)	17.65	Nd < 0,10.Ac.fck conditio
+Y	C510 (8.53)+C410 (9.67)	18.2	B410 (8.35)+B439 (4.29)	15.17	Nd < 0,10.Ac.fck conditio
-Y	C510 (8.53)+C410 (9.67)	18.2	B410 (4.29)+B439 (8.35)	15.17	Nd < 0,10.Ac.fck conditio
+X	C410 (9.66)+C310 (10.44)	20.09	B304 (8.35)+B305 (4.29)	15.18	✓
-X	C410 (9.66)+C310 (10.44)	20.09	B304 (6.35)+B305 (8.35)	17.65	✓
+Y	C410 (9.67)+C310 (10.48)	20.16	B310 (10.3)+B339 (6.35)	19.98	✓
-Y	C410 (9.67)+C310 (10.48)	20.16	B310 (6.35)+B339 (10.3)	19.98	✓

STRONG COLUMN CHECK (tm)

Dir	Column	Mrc	Beam	Mrb	EXPLANATION
+X	C514 (4.06)	4.06	B529 (4.29)+B530 (8.35)	15.17	Bldg. upper level cnd.
-X	C514 (4.06)	4.06	B529 (8.35)+B530 (4.29)	15.17	Bldg. upper level cnd.
+Y	C514 (6.14)	6.14	B526 (4.29)	5.14	Bldg. upper level cnd.
-Y	C514 (6.14)	6.14	B526 (8.35)	10.02	Bldg. upper level cnd.
+X	C514 (4.06)+C414 (4.82)	8.88	B429 (4.29)+B430 (8.35)	15.17	Nd < 0,10.Ac.fck conditio
-X	C514 (4.06)+C414 (4.82)	8.88	B429 (8.35)+B430 (4.29)	15.17	Nd < 0,10.Ac.fck conditio
+Y	C514 (6.14)+C414 (7.31)	13.45	B426 (4.29)	5.14	✓
-Y	C514 (6.14)+C414 (7.31)	13.45	B426 (8.35)	10.02	✓
+X	C414 (4.82)+C314 (5.52)	10.34	B329 (4.29)+B330 (8.35)	15.17	INSUFFICIENT!
-X	C414 (4.82)+C314 (5.52)	10.34	B329 (8.35)+B330 (4.29)	15.17	INSUFFICIENT!
+Y	C414 (7.31)+C314 (7.81)	15.12	B326 (6.35)	7.62	✓
-Y	C414 (7.31)+C314 (7.81)	15.12	B326 (8.35)	10.02	✓
+X	C314 (5.52)+C214 (6.2)	11.72	BZ29 (4.29)+BZ30 (8.35)	15.17	INSUFFICIENT!
-X	C314 (5.52)+C214 (6.2)	11.72	BZ29 (8.35)+BZ30 (4.29)	15.17	INSUFFICIENT!
+Y	C314 (7.81)+C214 (8.2)	16.01	BZ26 (4.29)	5.14	✓
-Y	C314 (7.81)+C214 (8.2)	16.01	BZ26 (8.35)	10.02	✓
+X	CZ14 (6.2)+CB14 (3.8)	10	BB29 (4.29)+BB30 (8.35)	15.17	Panel end zone
-X	CZ14 (6.2)+CB14 (3.8)	10	BB29 (8.35)+BB30 (4.29)	15.17	Panel end zone
+Y	CZ14 (8.2)+CB14 (5.73)	13.93	BB26 (4.29)	5.14	Panel end zone
-Y	CZ14 (8.2)+CB14 (5.73)	13.93	BB26 (8.35)	10.02	Panel end zone
+X	C515 (6)	6	B518 (7.08)	8.5	Bldg. upper level cnd.
-X	C515 (6)	6	B518 (6.35)	7.63	Bldg. upper level cnd.
+Y	C515 (3.95)	3.95	B531 (8.35)+B532 (4.29)	15.17	Bldg. upper level cnd.
-Y	C515 (3.95)	3.95	B531 (4.29)+B532 (8.35)	15.17	Bldg. upper level cnd.
+X	C515 (6)+C415 (7.15)	13.15	B418 (7.08)	8.5	Nd < 0,10.Ac.fck conditio
-X	C515 (6)+C415 (7.15)	13.15	B418 (6.35)	7.63	Nd < 0,10.Ac.fck conditio
+Y	C515 (3.95)+C415 (4.77)	8.73	B431 (8.35)+B432 (4.29)	15.17	Nd < 0,10.Ac.fck conditio
-Y	C515 (3.95)+C415 (4.77)	8.73	B431 (4.29)+B432 (8.35)	15.17	Nd < 0,10.Ac.fck conditio
+X	C415 (7.15)+C315 (7.73)	14.88	B318 (7.91)	9.51	✓
-X	C415 (7.15)+C315 (7.73)	14.88	B318 (6.35)	7.63	✓
+Y	C415 (4.77)+C315 (5.49)	10.26	B331 (8.35)+B332 (4.29)	15.17	INSUFFICIENT!
-Y	C415 (4.77)+C315 (5.49)	10.26	B331 (4.29)+B332 (8.35)	15.17	INSUFFICIENT!
+X	C315 (7.73)+C215 (8.15)	15.88	BZ18 (7.91)	9.51	✓
-X	C315 (7.73)+C215 (8.15)	15.88	BZ18 (6.35)	7.63	✓
+Y	C315 (5.49)+C215 (6.09)	11.58	BZ31 (8.35)+BZ32 (4.29)	15.17	INSUFFICIENT!
-Y	C315 (5.49)+C215 (6.09)	11.58	BZ31 (4.29)+BZ32 (8.35)	15.17	INSUFFICIENT!
+X	CZ15 (8.15)+CB15 (5.32)	13.48	BB18 (7.08)	8.5	Panel end zone
-X	CZ15 (8.15)+CB15 (5.32)	13.48	BB18 (6.35)	7.63	Panel end zone
+Y	CZ15 (6.09)+CB15 (3.73)	9.83	BB31 (8.35)+BB32 (4.29)	15.17	Panel end zone
-Y	CZ15 (6.09)+CB15 (3.73)	9.83	BB31 (4.29)+BB32 (8.35)	15.17	Panel end zone
+X	C516 (6.03)	6.03	B521 (7.08)	8.5	Bldg. upper level cnd.
-X	C516 (6.03)	6.03	B521 (6.35)	7.63	Bldg. upper level cnd.
+Y	C516 (4.01)	4.01	B532 (8.35)+B558 (4.29)	15.17	Bldg. upper level cnd.
-Y	C516 (4.01)	4.01	B532 (4.29)+B558 (8.35)	15.17	Bldg. upper level cnd.
+X	C516 (6.03)+C416 (7.22)	13.25	B421 (7.08)	8.5	Nd < 0,10.Ac.fck conditio
-X	C516 (6.03)+C416 (7.22)	13.25	B421 (6.35)	7.63	Nd < 0,10.Ac.fck conditio
+Y	C516 (4.01)+C416 (4.75)	8.76	B432 (8.35)+B458 (4.29)	15.17	Nd < 0,10.Ac.fck conditio
-Y	C516 (4.01)+C416 (4.75)	8.76	B432 (4.29)+B458 (8.35)	15.17	Nd < 0,10.Ac.fck conditio
+X	C416 (7.22)+C316 (7.76)	14.98	B321 (7.08)	8.5	✓
-X	C416 (7.22)+C316 (7.76)	14.98	B321 (6.35)	7.63	✓
+Y	C416 (4.75)+C316 (5.43)	10.18	B332 (8.35)+B358 (4.29)	15.17	INSUFFICIENT!
-Y	C416 (4.75)+C316 (5.43)	10.18	B332 (4.29)+B358 (8.35)	15.17	INSUFFICIENT!
+X	C316 (7.76)+C216 (8.18)	15.94	BZ21 (7.91)	9.51	✓
-X	C316 (7.76)+C216 (8.18)	15.94	BZ21 (6.35)	7.63	✓
+Y	C316 (5.43)+C216 (5.99)	11.41	BZ32 (8.35)+BZ58 (4.29)	15.17	INSUFFICIENT!
-Y	C316 (5.43)+C216 (5.99)	11.41	BZ32 (4.29)+BZ58 (8.35)	15.17	INSUFFICIENT!
+X	CZ16 (8.18)+CB16 (5.38)	13.55	BB21 (7.08)	8.5	Panel end zone
-X	CZ16 (8.18)+CB16 (5.38)	13.55	BB21 (6.35)	7.63	Panel end zone
+Y	CZ16 (5.99)+CB16 (3.75)	9.74	BB32 (8.35)+BB58 (4.29)	15.17	Panel end zone
-Y	CZ16 (5.99)+CB16 (3.75)	9.74	BB32 (4.29)+BB58 (8.35)	15.17	Panel end zone
+X	C517 (8.49)	8.49	B518 (6.35)+B519 (8.35)	17.65	Bldg. upper level cnd.
-X	C517 (8.49)	8.49	B518 (8.35)+B519 (4.29)	15.18	Bldg. upper level cnd.
+Y	C517 (8.49)	8.49	B524 (8.35)+B525 (4.29)	15.17	Bldg. upper level cnd.
-Y	C517 (8.49)	8.49	B524 (4.29)+B525 (8.35)	15.17	Bldg. upper level cnd.
+X	C517 (8.49)+C417 (9.54)	18.03	B418 (6.35)+B419 (8.35)	17.65	Nd < 0,10.Ac.fck conditio
-X	C517 (8.49)+C417 (9.54)	18.03	B418 (8.35)+B419 (4.29)	15.18	Nd < 0,10.Ac.fck conditio
+Y	C517 (8.49)+C417 (9.58)	18.07	B424 (8.35)+B425 (4.29)	15.17	Nd < 0,10.Ac.fck conditio
-Y	C517 (8.49)+C417 (9.58)	18.07	B424 (4.29)+B425 (8.35)	15.17	Nd < 0,10.Ac.fck conditio

STRONG COLUMN CHECK (tm)

Dir	Column	Mrc	Beam	Mrb	EXPLANATION
+X	CZ20 (5.37)+CB20 (3.87)	9.25	BB42 (6.35)	7.62	Panel end zone
-X	CZ20 (5.37)+CB20 (3.87)	9.25	BB42 (7.08)	8.5	Panel end zone
+Y	CZ20 (7.49)+CB20 (5.14)	12.63	BB45 (8.35)	10.02	Panel end zone
-Y	CZ20 (7.49)+CB20 (5.14)	12.63	BB45 (6.35)	7.62	Panel end zone
+X	C521 (3.95)	3.95	B542 (8.35)+B543 (4.29)	15.17	Bldg. upper level cnd.
-X	C521 (3.95)	3.95	B542 (6.35)+B543 (8.35)	17.64	Bldg. upper level cnd.
+Y	C521 (5.99)	5.99	B538 (8.35)	10.02	Bldg. upper level cnd.
-Y	C521 (5.99)	5.99	B538 (4.29)	5.14	Bldg. upper level cnd.
+X	C521 (3.95)+C421 (4.6)	8.55	B442 (8.35)+B443 (4.29)	15.17	Nd < 0,10.Ac.fck conditio
-X	C521 (3.95)+C421 (4.6)	8.55	B442 (6.35)+B443 (8.35)	17.64	Nd < 0,10.Ac.fck conditio
+Y	C521 (5.99)+C421 (7.13)	13.11	B438 (8.35)	10.02	Nd < 0,10.Ac.fck conditio
-Y	C521 (5.99)+C421 (7.13)	13.11	B438 (4.29)	5.14	Nd < 0,10.Ac.fck conditio
+X	C421 (4.6)+C321 (5.17)	9.76	B342 (8.35)+B343 (4.29)	15.17	INSUFFICIENT!
-X	C421 (4.6)+C321 (5.17)	9.76	B342 (6.35)+B343 (8.35)	17.64	INSUFFICIENT!
+Y	C421 (7.13)+C321 (7.69)	14.82	B338 (9.06)	10.88	✓
-Y	C421 (7.13)+C321 (7.69)	14.82	B338 (6.35)	7.62	✓
+X	C321 (5.17)+CZ21 (5.67)	10.84	BZ42 (8.35)+BZ43 (4.29)	15.17	INSUFFICIENT!
-X	C321 (5.17)+CZ21 (5.67)	10.84	BZ42 (6.35)+BZ43 (8.35)	17.64	INSUFFICIENT!
+Y	C321 (7.69)+CZ21 (8.11)	15.8	BZ38 (9.06)	10.88	✓
-Y	C321 (7.69)+CZ21 (8.11)	15.8	BZ38 (6.35)	7.62	✓
+X	CZ21 (5.67)+CB21 (3.73)	9.4	BB42 (8.35)+BB43 (4.29)	15.17	Panel end zone
-X	CZ21 (5.67)+CB21 (3.73)	9.4	BB42 (6.35)+BB43 (8.35)	17.64	Panel end zone
+Y	CZ21 (8.11)+CB21 (5.32)	13.43	BB38 (8.35)	10.02	Panel end zone
-Y	CZ21 (8.11)+CB21 (5.32)	13.43	BB38 (4.29)	5.14	Panel end zone
+X	C522 (4.08)	4.08	B543 (8.35)+B544 (4.29)	15.17	Bldg. upper level cnd.
-X	C522 (4.08)	4.08	B543 (4.29)+B544 (8.35)	15.17	Bldg. upper level cnd.
+Y	C522 (6.13)	6.13	B540 (8.35)	10.02	Bldg. upper level cnd.
-Y	C522 (6.13)	6.13	B540 (4.29)	5.14	Bldg. upper level cnd.
+X	C522 (4.08)+C422 (4.88)	8.96	B443 (8.35)+B444 (4.29)	15.17	Nd < 0,10.Ac.fck conditio
-X	C522 (4.08)+C422 (4.88)	8.96	B443 (4.29)+B444 (8.35)	15.17	Nd < 0,10.Ac.fck conditio
+Y	C522 (6.13)+C422 (7.3)	13.43	B440 (8.35)	10.02	✓
-Y	C522 (6.13)+C422 (7.3)	13.43	B440 (4.29)	5.14	✓
+X	C422 (4.88)+C322 (5.6)	10.47	B343 (8.35)+B344 (4.29)	15.17	INSUFFICIENT!
-X	C422 (4.88)+C322 (5.6)	10.47	B343 (4.29)+B344 (8.35)	15.17	INSUFFICIENT!
+Y	C422 (7.3)+C322 (7.81)	15.12	B340 (8.35)	10.02	✓
-Y	C422 (7.3)+C322 (7.81)	15.12	B340 (6.35)	7.62	✓
+X	C322 (5.6)+CZ22 (6.18)	11.77	BZ43 (8.35)+BZ44 (4.29)	15.17	INSUFFICIENT!
-X	C322 (5.6)+CZ22 (6.18)	11.77	BZ43 (4.29)+BZ44 (8.35)	15.17	INSUFFICIENT!
+Y	C322 (7.81)+CZ22 (8.21)	16.03	BZ40 (8.35)	10.02	✓
-Y	C322 (7.81)+CZ22 (8.21)	16.03	BZ40 (6.35)	7.62	✓
+X	CZ22 (6.18)+CB22 (3.79)	9.97	BB43 (8.35)+BB44 (4.29)	15.17	Panel end zone
-X	CZ22 (6.18)+CB22 (3.79)	9.97	BB43 (4.29)+BB44 (8.35)	15.17	Panel end zone
+Y	CZ22 (8.21)+CB22 (5.44)	13.65	BB40 (8.35)	10.02	Panel end zone
-Y	CZ22 (8.21)+CB22 (5.44)	13.65	BB40 (4.29)	5.14	Panel end zone
+X	C523 (4.1)	4.1	B544 (8.35)+B556 (4.29)	15.17	Bldg. upper level cnd.
-X	C523 (4.1)	4.1	B544 (4.29)+B556 (8.35)	15.17	Bldg. upper level cnd.
+Y	C523 (6.16)	6.16	B536 (8.35)	10.02	Bldg. upper level cnd.
-Y	C523 (6.16)	6.16	B536 (4.29)	5.14	Bldg. upper level cnd.
+X	C523 (4.1)+C423 (4.9)	9	B444 (8.35)+B456 (4.29)	15.17	Nd < 0,10.Ac.fck conditio
-X	C523 (4.1)+C423 (4.9)	9	B444 (4.29)+B456 (8.35)	15.17	Nd < 0,10.Ac.fck conditio
+Y	C523 (6.16)+C423 (7.32)	13.47	B436 (8.35)	10.02	✓
-Y	C523 (6.16)+C423 (7.32)	13.47	B436 (4.29)	5.14	✓
+X	C423 (4.9)+C323 (5.62)	10.52	B344 (8.35)+B356 (4.29)	15.17	INSUFFICIENT!
-X	C423 (4.9)+C323 (5.62)	10.52	B344 (4.29)+B356 (8.35)	15.17	INSUFFICIENT!
+Y	C423 (7.32)+C323 (7.82)	15.14	B336 (8.35)	10.02	✓
-Y	C423 (7.32)+C323 (7.82)	15.14	B336 (6.35)	7.62	✓
+X	C323 (5.62)+CZ23 (6.2)	11.82	BZ44 (8.35)+BZ56 (4.29)	15.17	INSUFFICIENT!
-X	C323 (5.62)+CZ23 (6.2)	11.82	BZ44 (4.29)+BZ56 (8.35)	15.17	INSUFFICIENT!
+Y	C323 (7.82)+CZ23 (8.21)	16.04	BZ36 (8.35)	10.02	✓
-Y	C323 (7.82)+CZ23 (8.21)	16.04	BZ36 (4.29)	5.14	✓
+X	CZ23 (6.2)+CB23 (3.8)	10	BB44 (8.35)+BB56 (4.29)	15.17	Panel end zone
-X	CZ23 (6.2)+CB23 (3.8)	10	BB44 (4.29)+BB56 (8.35)	15.17	Panel end zone
+Y	CZ23 (8.21)+CB23 (5.49)	13.7	BB36 (8.35)	10.02	Panel end zone
-Y	CZ23 (8.21)+CB23 (5.49)	13.7	BB36 (4.29)	5.14	Panel end zone
+X	C524 (5.98)	5.98	B533 (6.35)	7.63	Bldg. upper level cnd.
-X	C524 (5.98)	5.98	B533 (7.08)	8.5	Bldg. upper level cnd.
+Y	C524 (3.95)	3.95	B545 (4.29)+B546 (8.35)	15.17	Bldg. upper level cnd.
-Y	C524 (3.95)	3.95	B545 (8.35)+B546 (4.29)	15.17	Bldg. upper level cnd.

STRONG COLUMN CHECK (tm)

Dir	Column	Mrc	Beam	Mrb	EXPLANATION
+X	C524 (5.98)+C424 (7.14)	13.12	B433 (6.35)	7.63	Nd < 0,10.Ac.fck conditio
-X	C524 (5.98)+C424 (7.14)	13.12	B433 (7.08)	8.5	Nd < 0,10.Ac.fck conditio
+Y	C524 (3.95)+C424 (4.58)	8.53	B445 (4.29)+B446 (8.35)	15.17	Nd < 0,10.Ac.fck conditio
-Y	C524 (3.95)+C424 (4.58)	8.53	B445 (8.35)+B446 (4.29)	15.17	Nd < 0,10.Ac.fck conditio
+X	C424 (7.14)+C324 (7.72)	14.85	B333 (6.35)	7.63	✓
-X	C424 (7.14)+C324 (7.72)	14.85	B333 (7.91)	9.51	✓
+Y	C424 (4.58)+C324 (5.14)	9.72	B345 (4.29)+B346 (8.35)	15.17	INSUFFICIENT!
-Y	C424 (4.58)+C324 (5.14)	9.72	B345 (8.35)+B346 (4.29)	15.17	INSUFFICIENT!
+X	C324 (7.72)+CZ24 (8.15)	15.86	BZ33 (6.35)	7.63	✓
-X	C324 (7.72)+CZ24 (8.15)	15.86	BZ33 (7.91)	9.51	✓
+Y	C324 (5.14)+CZ24 (6.13)	11.27	BZ45 (4.29)+BZ46 (8.35)	15.17	INSUFFICIENT!
-Y	C324 (5.14)+CZ24 (6.13)	11.27	BZ45 (8.35)+BZ46 (4.29)	15.17	INSUFFICIENT!
+X	CZ24 (8.15)+CB24 (5.68)	13.82	BB33 (6.35)	7.63	Panel end zone
-X	CZ24 (8.15)+CB24 (5.68)	13.82	BB33 (7.08)	8.5	Panel end zone
+Y	CZ24 (6.13)+CB24 (3.74)	9.87	BB45 (4.29)+BB46 (8.35)	15.17	Panel end zone
-Y	CZ24 (6.13)+CB24 (3.74)	9.87	BB45 (8.35)+BB46 (4.29)	15.17	Panel end zone
+X	C525 (8.52)	8.52	B533 (8.35)+B534 (4.29)	15.18	Bldg. upper level cnd.
-X	C525 (8.52)	8.52	B533 (6.35)+B534 (8.35)	17.65	Bldg. upper level cnd.
+Y	C525 (8.49)	8.49	B538 (4.29)+B539 (8.35)	15.17	Bldg. upper level cnd.
-Y	C525 (8.49)	8.49	B538 (8.35)+B539 (4.29)	15.17	Bldg. upper level cnd.
+X	C525 (8.52)+C425 (9.6)	18.11	B433 (8.35)+B434 (4.29)	15.18	Nd < 0,10.Ac.fck conditio
-X	C525 (8.52)+C425 (9.6)	18.11	B433 (6.35)+B434 (8.35)	17.65	Nd < 0,10.Ac.fck conditio
+Y	C525 (8.49)+C425 (9.59)	18.08	B438 (4.29)+B439 (8.35)	15.17	Nd < 0,10.Ac.fck conditio
-Y	C525 (8.49)+C425 (9.59)	18.08	B438 (8.35)+B439 (4.29)	15.17	Nd < 0,10.Ac.fck conditio
+X	C425 (9.6)+C325 (10.38)	19.98	B333 (8.35)+B334 (4.29)	15.18	✓
-X	C425 (9.6)+C325 (10.38)	19.98	B333 (6.35)+B334 (8.35)	17.65	✓
+Y	C425 (9.59)+C325 (10.4)	19.99	B338 (6.35)+B339 (10.3)	19.98	✓
-Y	C425 (9.59)+C325 (10.4)	19.99	B338 (10.3)+B339 (6.35)	19.98	✓
+X	C325 (10.38)+CZ25 (10.88)	21.26	BZ33 (8.35)+BZ34 (4.29)	15.18	✓
-X	C325 (10.38)+CZ25 (10.88)	21.26	BZ33 (6.35)+BZ34 (8.35)	17.65	✓
+Y	C325 (10.4)+CZ25 (10.93)	21.33	BZ38 (6.35)+BZ39 (8.35)	17.64	✓
-Y	C325 (10.4)+CZ25 (10.93)	21.33	BZ38 (8.35)+BZ39 (6.35)	17.64	✓
+X	CZ25 (10.88)+CB25 (11.45)	22.33	BB33 (8.35)+BB34 (4.29)	15.18	Basement
-X	CZ25 (10.88)+CB25 (11.45)	22.33	BB33 (6.35)+BB34 (8.35)	17.65	Basement
+Y	CZ25 (10.93)+CB25 (11.4)	22.33	BB38 (4.29)+BB39 (8.35)	15.17	Basement
-Y	CZ25 (10.93)+CB25 (11.4)	22.33	BB38 (8.35)+BB39 (4.29)	15.17	Basement
+X	C526 (8.61)	8.61	B534 (8.35)+B535 (4.29)	15.18	Bldg. upper level cnd.
-X	C526 (8.61)	8.61	B534 (4.29)+B535 (8.35)	15.18	Bldg. upper level cnd.
+Y	C526 (8.64)	8.64	B540 (4.29)+B541 (8.35)	15.17	Bldg. upper level cnd.
-Y	C526 (8.64)	8.64	B540 (8.35)+B541 (4.29)	15.17	Bldg. upper level cnd.
+X	C526 (8.61)+C426 (9.8)	18.41	B434 (8.35)+B435 (4.29)	15.18	Nd < 0,10.Ac.fck conditio
-X	C526 (8.61)+C426 (9.8)	18.41	B434 (4.29)+B435 (8.35)	15.18	Nd < 0,10.Ac.fck conditio
+Y	C526 (8.64)+C426 (9.85)	18.49	B440 (4.29)+B441 (8.35)	15.17	Nd < 0,10.Ac.fck conditio
-Y	C526 (8.64)+C426 (9.85)	18.49	B440 (8.35)+B441 (4.29)	15.17	Nd < 0,10.Ac.fck conditio
+X	C426 (9.8)+C326 (10.6)	20.41	B334 (8.35)+B335 (4.29)	15.18	✓
-X	C426 (9.8)+C326 (10.6)	20.41	B334 (4.29)+B335 (8.35)	15.18	✓
+Y	C426 (9.85)+C326 (10.63)	20.48	B340 (4.29)+B341 (8.35)	15.17	✓
-Y	C426 (9.85)+C326 (10.63)	20.48	B340 (8.35)+B341 (4.29)	15.17	✓
+X	C326 (10.6)+CZ26 (11.17)	21.77	BZ34 (8.35)+BZ35 (4.29)	15.18	✓
-X	C326 (10.6)+CZ26 (11.17)	21.77	BZ34 (4.29)+BZ35 (8.35)	15.18	✓
+Y	C326 (10.63)+CZ26 (11.19)	21.82	BZ40 (4.29)+BZ41 (8.35)	15.17	✓
-Y	C326 (10.63)+CZ26 (11.19)	21.82	BZ40 (8.35)+BZ41 (4.29)	15.17	✓
+X	CZ26 (11.17)+CB26 (11.61)	22.78	BB34 (8.35)+BB35 (4.29)	15.18	Basement
-X	CZ26 (11.17)+CB26 (11.61)	22.78	BB34 (4.29)+BB35 (8.35)	15.18	Basement
+Y	CZ26 (11.19)+CB26 (11.6)	22.79	BB40 (4.29)+BB41 (8.35)	15.17	Basement
-Y	CZ26 (11.19)+CB26 (11.6)	22.79	BB40 (8.35)+BB41 (4.29)	15.17	Basement
+X	C527 (8.39)	8.39	B535 (8.35)+B549 (4.29)	15.18	Bldg. upper level cnd.
-X	C527 (8.39)	8.39	B535 (4.29)+B549 (8.35)	15.18	Bldg. upper level cnd.
+Y	C527 (8.19)	8.19	B536 (4.29)+B537 (8.35)	15.17	Bldg. upper level cnd.
-Y	C527 (8.19)	8.19	B536 (8.35)+B537 (6.35)	17.64	Bldg. upper level cnd.
+X	C527 (8.39)+C427 (9.47)	17.86	B435 (8.35)+B449 (4.29)	15.18	Nd < 0,10.Ac.fck conditio
-X	C527 (8.39)+C427 (9.47)	17.86	B435 (4.29)+B449 (8.35)	15.18	Nd < 0,10.Ac.fck conditio
+Y	C527 (8.19)+C427 (9.15)	17.34	B436 (6.35)+B437 (8.35)	17.64	Nd < 0,10.Ac.fck conditio
-Y	C527 (8.19)+C427 (9.15)	17.34	B436 (8.35)+B437 (8.35)	20.05	Nd < 0,10.Ac.fck conditio
+X	C427 (9.47)+C327 (10.33)	19.79	B335 (10.3)+B349 (6.35)	19.99	INSUFFICIENT!
-X	C427 (9.47)+C327 (10.33)	19.79	B335 (6.35)+B349 (10.3)	20	INSUFFICIENT!
+Y	C427 (9.15)+C327 (9.96)	19.11	B336 (6.35)+B337 (8.35)	17.64	Nd < 0,10.Ac.fck conditio
-Y	C427 (9.15)+C327 (9.96)	19.11	B336 (8.35)+B337 (8.35)	20.05	Nd < 0,10.Ac.fck conditio

STRONG COLUMN CHECK (tm)

Dir	Column	Mrc	Beam	Mrb	EXPLANATION
+X	C534 (194.62)+C434 (216.13)	410.75	B408 (16.8)+B423 (8.35)+B459 (8.3	40.23	Nd < 0,10.Ac.fck conditio
-X	C534 (179.74)+C434 (194.23)	373.97	B408 (7.08)+B423 (11.36)+B459 (11	35.79	Nd < 0,10.Ac.fck conditio
+Y	C534 (206.76)+C434 (226.14)	432.9	B407 (15.04)+B437 (8.35)	28.07	Nd < 0,10.Ac.fck conditio
-Y	C534 (207.42)+C434 (226.27)	433.69	B407 (8.35)+B437 (15.04)	28.07	Nd < 0,10.Ac.fck conditio
+X	C434 (216.13)+C334 (237.45)	453.59	B308 (16.8)+B323 (9.87)+B359 (9.8	43.88	Nd < 0,10.Ac.fck conditio
-X	C434 (194.23)+C334 (226.14)	420.37	B308 (7.91)+B323 (15.04)+B359 (15	45.62	Nd < 0,10.Ac.fck conditio
+Y	C434 (226.14)+C334 (294.3)	520.44	B307 (15.04)+B337 (8.35)	28.07	Nd < 0,10.Ac.fck conditio
-Y	C434 (226.27)+C334 (278.42)	504.69	B307 (8.35)+B337 (15.04)	28.07	Nd < 0,10.Ac.fck conditio
+X	C334 (237.45)+CZ34 (284.92)	522.37	BZ08 (16.8)+BZ23 (11.78)+BZ59 (11	48.46	Nd < 0,10.Ac.fck conditio
-X	C334 (226.14)+CZ34 (219.78)	445.92	BZ08 (7.91)+BZ23 (15.04)+BZ59 (15	45.62	Nd < 0,10.Ac.fck conditio
+Y	C334 (294.3)+CZ34 (297.64)	591.93	BZ07 (15.04)+BZ37 (8.35)	28.07	Nd < 0,10.Ac.fck conditio
-Y	C334 (278.42)+CZ34 (329.18)	607.6	BZ07 (8.35)+BZ37 (15.04)	28.07	Nd < 0,10.Ac.fck conditio
+X	CZ34 (284.92)+CB34 (311.29)	596.21	BB08 (8.35)+BB23 (6.35)+BB59 (6.3	25.27	Basement
-X	CZ34 (219.78)+CB34 (253.2)	472.98	BB08 (4.29)+BB23 (7.08)+BB59 (7.0	22.14	Basement
+Y	CZ34 (297.64)+CB34 (300.77)	598.41	BB07 (7.08)+BB37 (6.35)	16.11	Basement
-Y	CZ34 (329.18)+CB34 (332.15)	661.33	BB07 (6.35)+BB37 (7.08)	16.11	Basement
+X	C635 (16.36)	16.36	B623 (7.08)+B659 (7.08)	16.98	Bldg. upper level cnd.
-X	C635 (16.36)	16.36	B623 (6.35)+B659 (6.35)	15.23	Bldg. upper level cnd.
+Y	C635 (130.55)	130.55		0	Bldg. upper level cnd.
-Y	C635 (130.55)	130.55		0	Bldg. upper level cnd.
+X	C635 (16.36)+C535 (17.53)	33.88	B522 (4.29)+B523 (7.08)+B559 (7.0	22.15	Bldg. upper level cnd.
-X	C635 (16.36)+C535 (17.53)	33.88	B522 (8.35)+B523 (6.35)+B559 (6.3	25.27	Bldg. upper level cnd.
+Y	C635 (130.55)+C535 (140.72)	271.28	B527 (15.04)+B553 (6.35)	25.67	Bldg. upper level cnd.
-Y	C635 (130.55)+C535 (140.72)	271.28	B527 (6.35)+B553 (15.04)	25.67	Bldg. upper level cnd.
+X	C535 (17.53)+C435 (18.53)	36.05	B422 (4.29)+B423 (7.08)+B459 (7.0	22.15	Nd < 0,10.Ac.fck conditio
-X	C535 (17.53)+C435 (18.53)	36.05	B422 (8.35)+B423 (6.35)+B459 (6.3	25.28	Nd < 0,10.Ac.fck conditio
+Y	C535 (140.72)+C435 (150.34)	291.06	B427 (15.04)+B453 (8.35)	28.07	Nd < 0,10.Ac.fck conditio
-Y	C535 (140.72)+C435 (150.34)	291.06	B427 (8.35)+B453 (15.04)	28.07	Nd < 0,10.Ac.fck conditio
+X	C435 (18.53)+C335 (19.24)	37.77	B322 (4.29)+B323 (7.08)+B359 (7.0	22.15	Nd < 0,10.Ac.fck conditio
-X	C435 (18.53)+C335 (19.24)	37.77	B322 (8.35)+B323 (6.35)+B359 (6.3	25.28	Nd < 0,10.Ac.fck conditio
+Y	C435 (150.34)+C335 (159.19)	309.53	B327 (15.04)+B353 (8.35)	28.07	Nd < 0,10.Ac.fck conditio
-Y	C435 (150.34)+C335 (159.19)	309.53	B327 (8.35)+B353 (15.04)	28.07	Nd < 0,10.Ac.fck conditio
+X	C335 (19.24)+CZ35 (19.73)	38.97	BZ22 (4.29)+BZ23 (7.08)+BZ59 (7.0	22.15	Nd < 0,10.Ac.fck conditio
-X	C335 (19.24)+CZ35 (19.73)	38.97	BZ22 (8.35)+BZ23 (6.35)+BZ59 (6.3	25.28	Nd < 0,10.Ac.fck conditio
+Y	C335 (159.19)+CZ35 (166.86)	326.05	BZ27 (15.04)+BZ53 (8.35)	28.07	Nd < 0,10.Ac.fck conditio
-Y	C335 (159.19)+CZ35 (166.86)	326.05	BZ27 (8.35)+BZ53 (15.04)	28.07	Nd < 0,10.Ac.fck conditio
+X	CZ35 (19.73)+CB35 (24.86)	44.59	BB22 (4.29)+BB23 (7.08)+BB59 (7.0	22.14	Basement
-X	CZ35 (19.73)+CB35 (24.86)	44.59	BB22 (8.35)+BB23 (6.35)+BB59 (6.3	25.27	Basement
+Y	CZ35 (166.86)+CB35 (173.05)	339.91	BB27 (7.08)+BB53 (6.35)	16.11	Basement
-Y	CZ35 (166.86)+CB35 (173.05)	339.91	BB27 (6.35)+BB53 (7.08)	16.11	Basement

COLUMNS SHEAR CHECK

$V_w = (A_{sw}/s) f_{ywd} d$, $V_c = 0.65 f_{ctd} A_c$, $V_r = 0.8 V_{cr} + V_w \geq V_d$ (t)

Column		Asw/s	Vw	Vcr	Vd	Vr=0.8 Vcr+ Vw
CB01	x	0.1507	13.761	6.631	0.038	19.066 ✓
CB01	y	0.1005	12.844	6.631	0.115	18.148 ✓
CB02	x	0.1884	17.202	6.631	0.040	22.506 ✓
CB02	y	0.1256	16.055	6.631	0.502	21.359 ✓
CB03	x	0.1507	13.761	6.631	0.044	19.066 ✓
CB03	y	0.1005	12.844	6.631	0.473	18.148 ✓
CB04	x	0.1507	13.761	6.631	0.043	19.066 ✓
CB04	y	0.1005	12.844	6.631	0.431	18.148 ✓
CB05	x	0.1005	12.844	6.631	0.412	18.148 ✓
CB05	y	0.1507	13.761	6.631	0.065	19.066 ✓
CB06	x	0.1005	12.844	6.631	0.401	18.148 ✓
CB06	y	0.1507	13.761	6.631	0.066	19.066 ✓
CB07	x	0.2010	29.358	9.518	0.375	36.972 ✓
CB07	y	0.2010	29.358	9.518	0.229	36.972 ✓
CB08	x	0.2010	29.358	9.518	0.182	36.972 ✓
CB08	y	0.2010	29.358	9.518	0.194	36.972 ✓
CB09	x	0.2010	29.358	9.518	0.215	36.972 ✓
CB09	y	0.2010	29.358	9.518	0.157	36.972 ✓
CB10	x	0.2010	29.358	9.518	0.371	36.972 ✓
CB10	y	0.2010	29.358	9.518	0.159	36.972 ✓
CB11	x	0.2010	29.358	9.518	0.176	36.972 ✓
CB11	y	0.2010	29.358	9.518	0.131	36.972 ✓
CB12	x	0.1507	13.761	6.631	0.038	19.066 ✓
CB12	y	0.1005	12.844	6.631	0.118	18.148 ✓
CB13	x	0.1507	13.761	6.631	0.041	19.066 ✓
CB13	y	0.1005	12.844	6.631	0.416	18.148 ✓
CB14	x	0.1507	13.761	6.631	0.044	19.066 ✓
CB14	y	0.1005	12.844	6.631	0.423	18.148 ✓
CB15	x	0.1005	12.844	6.631	0.408	18.148 ✓
CB15	y	0.1507	13.761	6.631	0.065	19.066 ✓
CB16	x	0.1005	12.844	6.631	0.396	18.148 ✓
CB16	y	0.1507	13.761	6.631	0.066	19.066 ✓
CB17	x	0.2010	29.358	9.518	0.351	36.972 ✓
CB17	y	0.2010	29.358	9.518	0.133	36.972 ✓
CB18	x	0.2010	29.358	9.518	0.195	36.972 ✓
CB18	y	0.2010	29.358	9.518	0.143	36.972 ✓
CB19	x	0.2010	29.358	9.518	0.291	36.972 ✓
CB19	y	0.2010	29.358	9.518	0.081	36.972 ✓
CB20	x	0.1507	13.761	6.631	0.038	19.066 ✓
CB20	y	0.1005	12.844	6.631	0.115	18.148 ✓
CB21	x	0.1507	13.761	6.631	0.040	19.066 ✓
CB21	y	0.1005	12.844	6.631	0.502	18.148 ✓
CB22	x	0.1507	13.761	6.631	0.044	19.066 ✓
CB22	y	0.1005	12.844	6.631	0.474	18.148 ✓
CB23	x	0.1507	13.761	6.631	0.043	19.066 ✓
CB23	y	0.1005	12.844	6.631	0.431	18.148 ✓
CB24	x	0.1005	12.844	6.631	0.412	18.148 ✓
CB24	y	0.1507	13.761	6.631	0.065	19.066 ✓
CB25	x	0.2010	29.358	9.518	0.375	36.972 ✓
CB25	y	0.2010	29.358	9.518	0.229	36.972 ✓
CB26	x	0.2010	29.358	9.518	0.182	36.972 ✓
CB26	y	0.2010	29.358	9.518	0.194	36.972 ✓
CB27	x	0.2010	29.358	9.518	0.215	36.972 ✓
CB27	y	0.2010	29.358	9.518	0.157	36.972 ✓
CB28	x	0.1507	13.761	6.631	0.038	19.066 ✓
CB28	y	0.1005	12.844	6.631	0.118	18.148 ✓
CB29	x	0.1507	13.761	6.631	0.041	19.066 ✓
CB29	y	0.1005	12.844	6.631	0.417	18.148 ✓
CB30	x	0.1507	13.761	6.631	0.044	19.066 ✓
CB30	y	0.1005	12.844	6.631	0.423	18.148 ✓
CB31	x	0.1005	12.844	6.631	0.408	18.148 ✓
CB31	y	0.1507	13.761	6.631	0.065	19.066 ✓
CB32	x	0.2010	29.358	9.518	0.351	36.972 ✓
CB32	y	0.2010	29.358	9.518	0.133	36.972 ✓
CB33	x	0.2010	29.358	9.518	0.195	36.972 ✓
CB33	y	0.2010	29.358	9.518	0.143	36.972 ✓
CB35	x	0.5582	50.968	31.259	0.452	75.975 ✓
CB35	y	0.1116	67.278	31.259	24.216	92.285 ✓
CZ01	x	0.1884	17.202	6.631	1.276	22.506 ✓
CZ01	y	0.1256	16.055	6.631	2.522	21.359 ✓
CZ02	x	0.1884	17.202	6.631	1.405	22.506 ✓
CZ02	y	0.1256	16.055	6.631	2.730	21.359 ✓
CZ03	x	0.1884	17.202	6.631	1.350	22.506 ✓
CZ03	y	0.1256	16.055	6.631	2.493	21.359 ✓
CZ04	x	0.1884	17.202	6.631	1.347	22.506 ✓
CZ04	y	0.1256	16.055	6.631	2.203	21.359 ✓
CZ05	x	0.1256	16.055	6.631	2.373	21.359 ✓
CZ05	y	0.1884	17.202	6.631	1.654	22.506 ✓
CZ06	x	0.1256	16.055	6.631	2.246	21.359 ✓
CZ06	y	0.1884	17.202	6.631	1.566	22.506 ✓
CZ07	x	0.2010	29.358	9.518	3.624	36.972 ✓
CZ07	y	0.2010	29.358	9.518	3.723	36.972 ✓

COLUMNS SHEAR CHECK

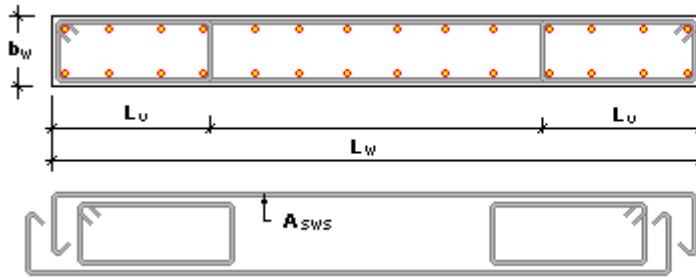
Column	Asw/s	Vw	Vcr	Vd	Vr=0.8 Vcr+ Vw	
C316	x	0.1256	16.055	6.631	2.501	21.359 ✓
C316	y	0.1884	17.202	6.631	1.526	22.506 ✓
C317	x	0.2010	29.358	9.518	4.181	36.972 ✓
C317	y	0.2010	29.358	9.518	3.588	36.972 ✓
C318	x	0.2010	29.358	9.518	3.774	36.972 ✓
C318	y	0.2010	29.358	9.518	4.354	36.972 ✓
C319	x	0.2010	29.358	9.518	3.778	36.972 ✓
C319	y	0.2010	29.358	9.518	3.404	36.972 ✓
C320	x	0.1884	17.202	6.631	1.595	22.506 ✓
C320	y	0.1256	16.055	6.631	2.608	21.359 ✓
C321	x	0.1884	17.202	6.631	1.847	22.506 ✓
C321	y	0.1256	16.055	6.631	2.864	21.359 ✓
C322	x	0.1884	17.202	6.631	1.715	22.506 ✓
C322	y	0.1256	16.055	6.631	2.703	21.359 ✓
C323	x	0.1884	17.202	6.631	1.695	22.506 ✓
C323	y	0.1256	16.055	6.631	2.475	21.359 ✓
C324	x	0.1256	16.055	6.631	2.606	21.359 ✓
C324	y	0.1884	17.202	6.631	2.031	22.506 ✓
C325	x	0.2010	29.358	9.518	4.218	36.972 ✓
C325	y	0.2010	29.358	9.518	4.199	36.972 ✓
C326	x	0.2010	29.358	9.518	3.827	36.972 ✓
C326	y	0.2010	29.358	9.518	3.761	36.972 ✓
C327	x	0.2010	29.358	9.518	3.789	36.972 ✓
C327	y	0.2010	29.358	9.518	4.359	36.972 ✓
C328	x	0.1884	17.202	6.631	1.609	22.506 ✓
C328	y	0.1256	16.055	6.631	2.261	21.359 ✓
C329	x	0.1884	17.202	6.631	1.869	22.506 ✓
C329	y	0.1256	16.055	6.631	2.552	21.359 ✓
C330	x	0.1884	17.202	6.631	1.736	22.506 ✓
C330	y	0.1256	16.055	6.631	2.518	21.359 ✓
C331	x	0.1256	16.055	6.631	2.622	21.359 ✓
C331	y	0.1884	17.202	6.631	1.672	22.506 ✓
C332	x	0.2010	29.358	9.518	4.181	36.972 ✓
C332	y	0.2010	29.358	9.518	3.587	36.972 ✓
C333	x	0.2010	29.358	9.518	3.774	36.972 ✓
C333	y	0.2010	29.358	9.518	4.354	36.972 ✓
C335	x	0.6280	57.339	31.259	6.731	82.346 ✓
C335	y	0.1256	75.688	31.259	15.703	100.695 ✓
C401	x	0.1884	17.202	6.631	1.393	22.506 ✓
C401	y	0.1256	16.055	6.631	2.312	21.359 ✓
C402	x	0.1884	17.202	6.631	1.624	22.506 ✓
C402	y	0.1256	16.055	6.631	2.522	21.359 ✓
C403	x	0.1884	17.202	6.631	1.492	22.506 ✓
C403	y	0.1256	16.055	6.631	2.419	21.359 ✓
C404	x	0.1884	17.202	6.631	1.465	22.506 ✓
C404	y	0.1256	16.055	6.631	2.285	21.359 ✓
C405	x	0.1256	16.055	6.631	2.164	21.359 ✓
C405	y	0.1884	17.202	6.631	1.811	22.506 ✓
C406	x	0.1256	16.055	6.631	2.068	21.359 ✓
C406	y	0.1884	17.202	6.631	1.662	22.506 ✓
C407	x	0.2010	29.358	9.518	3.605	36.972 ✓
C407	y	0.2010	29.358	9.518	3.708	36.972 ✓
C408	x	0.2010	29.358	9.518	3.311	36.972 ✓
C408	y	0.2010	29.358	9.518	3.364	36.972 ✓
C409	x	0.2010	29.358	9.518	3.281	36.972 ✓
C409	y	0.2010	29.358	9.518	4.173	36.972 ✓
C410	x	0.2010	29.358	9.518	3.464	36.972 ✓
C410	y	0.2010	29.358	9.518	3.604	36.972 ✓
C411	x	0.2010	29.358	9.518	3.926	36.972 ✓
C411	y	0.2010	29.358	9.518	3.233	36.972 ✓
C412	x	0.1884	17.202	6.631	1.413	22.506 ✓
C412	y	0.1256	16.055	6.631	2.099	21.359 ✓
C413	x	0.1884	17.202	6.631	1.655	22.506 ✓
C413	y	0.1256	16.055	6.631	2.345	21.359 ✓
C414	x	0.1884	17.202	6.631	1.521	22.506 ✓
C414	y	0.1256	16.055	6.631	2.339	21.359 ✓
C415	x	0.1256	16.055	6.631	2.184	21.359 ✓
C415	y	0.1884	17.202	6.631	1.613	22.506 ✓
C416	x	0.1256	16.055	6.631	2.081	21.359 ✓
C416	y	0.1884	17.202	6.631	1.468	22.506 ✓
C417	x	0.2010	29.358	9.518	3.564	36.972 ✓
C417	y	0.2010	29.358	9.518	3.330	36.972 ✓
C418	x	0.2010	29.358	9.518	3.247	36.972 ✓
C418	y	0.2010	29.358	9.518	4.159	36.972 ✓
C419	x	0.2010	29.358	9.518	3.184	36.972 ✓
C419	y	0.2010	29.358	9.518	3.201	36.972 ✓
C420	x	0.1884	17.202	6.631	1.393	22.506 ✓
C420	y	0.1256	16.055	6.631	2.312	21.359 ✓
C421	x	0.1884	17.202	6.631	1.624	22.506 ✓
C421	y	0.1256	16.055	6.631	2.522	21.359 ✓
C422	x	0.1884	17.202	6.631	1.492	22.506 ✓
C422	y	0.1256	16.055	6.631	2.420	21.359 ✓
C423	x	0.1884	17.202	6.631	1.465	22.506 ✓
C423	y	0.1256	16.055	6.631	2.286	21.359 ✓

COLUMNS SHEAR CHECK

Column		Asw/s	Vw	Vcr	Vd	Vr=0.8 Vcr+ Vw
C532	x	0.2010	29.358	9.518	2.835	36.972 ✓
C532	y	0.2010	29.358	9.518	3.018	36.972 ✓
C533	x	0.2010	29.358	9.518	2.588	36.972 ✓
C533	y	0.2010	29.358	9.518	4.119	36.972 ✓
C535	x	0.6280	57.339	31.259	4.297	82.346 ✓
C535	y	0.1256	75.688	31.259	4.391	100.695 ✓
C635	x	0.6280	57.339	31.259	3.138	82.346 ✓
C635	y	0.1256	75.688	31.259	1.987	100.695 ✓

SHEARWALL DESIGN CHECK

$V_r = A_{ch} (0.65 f_{ctd} + r_{sh} f_{yd})$ Wall shear design
 $V_{rh} = 0.22 f_{cd} A_{ch}$ Max. concrete shear design
 $r_{shx} = A_{sWS} \cdot (\sum L_{etrx}/s) / A_{ch}$ $r_{shy} = A_{sWS} \cdot (\sum L_{etry}/s) / A_{ch}$
 $V_{fr} = \mu N + f_{yd} A_{sd} =$ Working point friction shear force
 $N = N_g - N_e$ Min. Wall load
 $\mu = 1$ (rough surface $\geq 5mm$)



Dikdörtgen perdelerde

$$q_{sh} = \frac{2 \cdot A_{sWS}}{A_{ch}} \cdot \left(\frac{L_w}{s} + \frac{2 \cdot L_u}{s_u} \right)$$

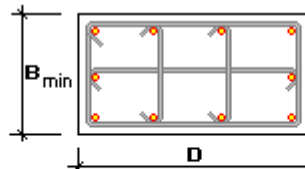
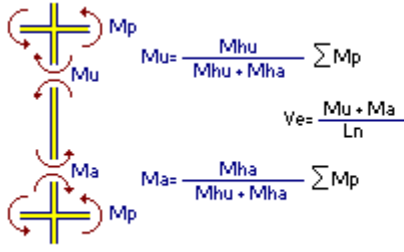
Poligon perdelerde

$$q_{shx} = \frac{A_{sWS}}{A_{ch}} \cdot \left(\sum \frac{L_{etrx}}{s} \right)$$

$$q_{shy} = \frac{A_{sWS}}{A_{ch}} \cdot \left(\sum \frac{L_{etry}}{s} \right)$$

$$V_r = 0.65 \cdot A_{ch} \cdot f_{ctd} + q \cdot A_{ch} \cdot f_{yd} > V_d$$

Column	Dir.	Ln	N	Vd	Vr	Vrh	Vfr	EXPLANATION	(t)
CB34	X	2.50	80.844	68.983	200.456	333.667	357.296	✓	
	Y	2.50	114.189	72.511	172.934	333.667	390.641	✓	
CZ34	X	2.50	64.651	59.369	200.456	333.667	357.972	✓	
	Y	2.50	94.758	58.817	172.934	333.667	388.080	✓	
C334	X	2.50	52.412	29.806	200.456	333.667	309.470	✓	
	Y	2.50	74.158	32.504	172.934	333.667	331.215	✓	
C434	X	2.50	38.903	17.687	200.456	333.667	249.599	✓	
	Y	2.50	52.734	17.266	172.934	333.667	263.429	✓	
C534	X	2.50	22.315	1.336	200.456	333.667	233.010	✓	
	Y	2.50	30.728	7.867	172.934	333.667	241.423	✓	
C634	X	2.50	4.717	1.109	200.456	333.667	215.413	✓	
	Y	3.00	9.240	3.314	172.934	333.667	219.936	✓	



Ln : Kolon kirişler arası serbest yükseklği
 Hk : Kolon kat yükseklği
 Fk : Kolon boyunca etriye alan toplamı
 $Letr$: hesap doğrultusundaki etriye boylarının toplamı

$$g = \frac{Fk \cdot Letr}{Ac \cdot Hk} \geq 0,0025$$

$$Vr = 0,65 \cdot Ac \cdot f_{ctd} + g \cdot Ac \cdot f_{yd} > Ve$$

Dikdörtgen kolonlarda $Letr \cong D$ $Ac = B \cdot D$

$$g = \frac{Fk \cdot D}{B \cdot D \cdot Hk} = \frac{Fk}{B \cdot Hk}$$

$$Vr = 0,65 \cdot B \cdot D \cdot f_{ctd} + Fk \cdot D \cdot f_{yd} / Hk > Ve$$

SHEAR DESIGN CHECK FOR COLUMNS

Column	+X			-X			+Y			-Y		
	Mp	Mc	Mr	Mp	Mc	Mr	Mp	Mc	Mr	Mp	Mc	Mr
CB07 Ln _x = 2.50 Ln _y = 2.50 Basement	10.88 12.65 + Mu= 6.49 11.45 0.00 + Ma= 11.45 0.00			10.88 -14.71 + Mu= 7.54 11.45 0.00 + Ma= 11.45 0.00			10.93 12.64 + Mu= 6.45 11.40 0.00 + Ma= 11.40 0.00			10.93 -12.64 + Mu= 6.45 11.40 0.00 + Ma= 11.40 0.00		
	Ve= 7.17 Vr= 38.88 ✓			Ve= 7.60 Vr= 38.88 ✓			Ve= 7.14 Vr= 38.88 ✓			Ve= 7.14 Vr= 38.88 ✓		
CB08 Ln _x = 2.50 Ln _y = 2.50 Basement	11.17 12.65 + Mu= 6.45 11.61 0.00 + Ma= 11.61 0.00			11.17 -12.65 + Mu= 6.45 11.61 0.00 + Ma= 11.61 0.00			11.19 12.64 + Mu= 6.43 11.60 0.00 + Ma= 11.60 0.00			11.19 -12.64 + Mu= 6.43 11.60 0.00 + Ma= 11.60 0.00		
	Ve= 7.22 Vr= 38.88 ✓			Ve= 7.22 Vr= 38.88 ✓			Ve= 7.22 Vr= 38.88 ✓			Ve= 7.22 Vr= 38.88 ✓		
CB09 Ln _x = 2.50 Ln _y = 2.50 Basement	10.94 12.65 + Mu= 6.45 11.37 0.00 + Ma= 11.37 0.00			10.94 -12.65 + Mu= 6.45 11.37 0.00 + Ma= 11.37 0.00			10.48 14.70 + Mu= 7.63 11.32 0.00 + Ma= 11.32 0.00			10.48 -12.64 + Mu= 6.56 11.32 0.00 + Ma= 11.32 0.00		
	Ve= 7.13 Vr= 38.88 ✓			Ve= 7.13 Vr= 38.88 ✓			Ve= 7.58 Vr= 38.88 ✓			Ve= 7.15 Vr= 38.88 ✓		
CB10 Ln _x = 2.50 Ln _y = 2.50 Basement	10.95 12.65 + Mu= 6.49 11.54 0.00 + Ma= 11.54 0.00			10.95 -14.71 + Mu= 7.55 11.54 0.00 + Ma= 11.54 0.00			11.04 12.64 + Mu= 6.43 11.44 0.00 + Ma= 11.44 0.00			11.04 -12.64 + Mu= 6.43 11.44 0.00 + Ma= 11.44 0.00		
	Ve= 7.21 Vr= 38.88 ✓			Ve= 7.63 Vr= 38.88 ✓			Ve= 7.15 Vr= 38.88 ✓			Ve= 7.15 Vr= 38.88 ✓		
CB11 Ln _x = 2.50 Ln _y = 2.50 Basement	10.98 12.65 + Mu= 6.52 11.67 0.00 + Ma= 11.67 0.00			10.98 -12.65 + Mu= 6.52 11.67 0.00 + Ma= 11.67 0.00			11.11 12.64 + Mu= 6.45 11.59 0.00 + Ma= 11.59 0.00			11.11 -12.64 + Mu= 6.45 11.59 0.00 + Ma= 11.59 0.00		
	Ve= 7.28 Vr= 38.88 ✓			Ve= 7.28 Vr= 38.88 ✓			Ve= 7.22 Vr= 38.88 ✓			Ve= 7.22 Vr= 38.88 ✓		
CB17 Ln _x = 2.50 Ln _y = 2.50 Basement	10.83 14.71 + Mu= 7.54 11.39 0.00 + Ma= 11.39 0.00			10.83 -12.65 + Mu= 6.48 11.39 0.00 + Ma= 11.39 0.00			10.93 12.64 + Mu= 6.42 11.30 0.00 + Ma= 11.30 0.00			10.93 -12.64 + Mu= 6.42 11.30 0.00 + Ma= 11.30 0.00		
	Ve= 7.57 Vr= 38.88 ✓			Ve= 7.15 Vr= 38.88 ✓			Ve= 7.09 Vr= 38.88 ✓			Ve= 7.09 Vr= 38.88 ✓		
CB18 Ln _x = 2.50 Ln _y = 2.50 Basement	10.93 12.65 + Mu= 6.45 11.36 0.00 + Ma= 11.36 0.00			10.93 -12.65 + Mu= 6.45 11.36 0.00 + Ma= 11.36 0.00			10.46 14.70 + Mu= 7.64 11.33 0.00 + Ma= 11.33 0.00			10.46 -12.64 + Mu= 6.57 11.33 0.00 + Ma= 11.33 0.00		
	Ve= 7.13 Vr= 38.88 ✓			Ve= 7.12 Vr= 38.88 ✓			Ve= 7.59 Vr= 38.88 ✓			Ve= 7.16 Vr= 38.88 ✓		
CB19 Ln _x = 2.50 Ln _y = 2.50 Basement	10.82 14.71 + Mu= 7.54 11.38 0.00 + Ma= 11.38 0.00			10.82 -12.65 + Mu= 6.48 11.38 0.00 + Ma= 11.38 0.00			10.88 12.64 + Mu= 6.44 11.31 0.00 + Ma= 11.31 0.00			10.88 -12.64 + Mu= 6.44 11.31 0.00 + Ma= 11.31 0.00		
	Ve= 7.57 Vr= 38.88 ✓			Ve= 7.14 Vr= 38.88 ✓			Ve= 7.10 Vr= 38.88 ✓			Ve= 7.10 Vr= 38.88 ✓		
CB25 Ln _x = 2.50 Ln _y = 2.50 Basement	10.88 12.65 + Mu= 6.49 11.45 0.00 + Ma= 11.45 0.00			10.88 -14.71 + Mu= 7.54 11.45 0.00 + Ma= 11.45 0.00			10.93 12.64 + Mu= 6.45 11.40 0.00 + Ma= 11.40 0.00			10.93 -12.64 + Mu= 6.45 11.40 0.00 + Ma= 11.40 0.00		
	Ve= 7.17 Vr= 38.88 ✓			Ve= 7.60 Vr= 38.88 ✓			Ve= 7.14 Vr= 38.88 ✓			Ve= 7.14 Vr= 38.88 ✓		
CB26 Ln _x = 2.50 Ln _y = 2.50 Basement	11.17 12.65 + Mu= 6.45 11.61 0.00 + Ma= 11.61 0.00			11.17 -12.65 + Mu= 6.45 11.61 0.00 + Ma= 11.61 0.00			11.19 12.64 + Mu= 6.43 11.60 0.00 + Ma= 11.60 0.00			11.19 -12.64 + Mu= 6.43 11.60 0.00 + Ma= 11.60 0.00		
	Ve= 7.22 Vr= 38.88 ✓			Ve= 7.22 Vr= 38.88 ✓			Ve= 7.22 Vr= 38.88 ✓			Ve= 7.22 Vr= 38.88 ✓		

SHEAR DESIGN CHECK FOR COLUMNS

Column	+X			-X			+Y			-Y		
	Mp	Mc	Mr	Mp	Mc	Mr	Mp	Mc	Mr	Mp	Mc	Mr
CZ21 Lnx= 2.50 Lny= 2.50	5.17			5.17			7.69			7.69		
	12.65	+	Mu= 5.67	-14.70	+	Mu= 5.67	9.06	+	Mu= 4.65	-6.35	+	Mu= 3.26
	0.01	+	Ma= 0.00	0.00	+	Ma= 0.00	8.35	+	Ma= 5.04	-4.29	+	Ma= 2.59
	3.73			3.73			5.32			5.32		
	Ve= 2.27		Vr= 23.83 ✓	Ve= 2.27		Vr= 23.83 ✓	Ve= 3.88		Vr= 22.69 ✓	Ve= 2.34		Vr= 22.69 ✓
CZ22 Lnx= 2.50 Lny= 2.50	5.60			5.60			7.81			7.81		
	12.64	+	Mu= 6.18	-12.64	+	Mu= 6.18	8.35	+	Mu= 4.28	-6.35	+	Mu= 3.25
	0.01	+	Ma= 0.00	0.00	+	Ma= 0.00	8.35	+	Ma= 5.03	-4.29	+	Ma= 2.58
	3.79			3.79			5.44			5.44		
	Ve= 2.47		Vr= 23.83 ✓	Ve= 2.47		Vr= 23.83 ✓	Ve= 3.72		Vr= 22.69 ✓	Ve= 2.33		Vr= 22.69 ✓
CZ23 Lnx= 2.50 Lny= 2.50	5.62			5.62			7.82			7.82		
	12.64	+	Mu= 6.20	-12.64	+	Mu= 6.20	8.35	+	Mu= 4.28	-4.29	+	Mu= 2.19
	0.01	+	Ma= 0.00	0.00	+	Ma= 0.00	8.35	+	Ma= 5.01	-4.29	+	Ma= 2.57
	3.80			3.80			5.49			5.49		
	Ve= 2.48		Vr= 23.83 ✓	Ve= 2.48		Vr= 23.83 ✓	Ve= 3.71		Vr= 22.69 ✓	Ve= 1.91		Vr= 22.69 ✓
CZ24 Lnx= 2.50 Lny= 2.50	7.72			7.72			5.14			5.14		
	6.36	+	Mu= 3.26	-7.92	+	Mu= 4.07	12.64	+	Mu= 6.13	-12.64	+	Mu= 6.13
	6.35	+	Ma= 3.74	-7.08	+	Ma= 4.17	0.00	+	Ma= 0.00	0.00	+	Ma= 0.00
	5.68			5.68			3.74			3.74		
	Ve= 2.80		Vr= 22.69 ✓	Ve= 3.30		Vr= 22.69 ✓	Ve= 2.45		Vr= 23.83 ✓	Ve= 2.45		Vr= 23.83 ✓
CZ25 Lnx= 2.50 Lny= 2.50	10.38			10.38			10.40			10.40		
	12.65	+	Mu= 6.47	-14.71	+	Mu= 7.53	14.70	+	Mu= 7.53	-14.70	+	Mu= 7.53
	12.65	+	Ma= 6.16	-14.71	+	Ma= 7.17	12.64	+	Ma= 6.19	-12.64	+	Ma= 6.19
	11.45			11.45			11.40			11.40		
	Ve= 5.05		Vr= 38.88 ✓	Ve= 5.88		Vr= 38.88 ✓	Ve= 5.49		Vr= 38.88 ✓	Ve= 5.49		Vr= 38.88 ✓
CZ26 Lnx= 2.50 Lny= 2.50	10.60			10.60			10.63			10.63		
	12.65	+	Mu= 6.49	-12.65	+	Mu= 6.49	12.64	+	Mu= 6.48	-12.64	+	Mu= 6.48
	12.65	+	Ma= 6.20	-12.65	+	Ma= 6.20	12.64	+	Ma= 6.20	-12.64	+	Ma= 6.20
	11.61			11.61			11.60			11.60		
	Ve= 5.08		Vr= 38.88 ✓	Ve= 5.08		Vr= 38.88 ✓	Ve= 5.07		Vr= 38.88 ✓	Ve= 5.07		Vr= 38.88 ✓
CZ27 Lnx= 2.50 Lny= 2.50	10.33			10.33			9.96			9.96		
	12.65	+	Mu= 6.49	-12.65	+	Mu= 6.49	14.70	+	Mu= 7.54	-16.70	+	Mu= 8.57
	12.65	+	Ma= 6.19	-12.65	+	Ma= 6.19	12.64	+	Ma= 6.07	-14.70	+	Ma= 7.07
	11.37			11.37			11.32			11.32		
	Ve= 5.07		Vr= 38.88 ✓	Ve= 5.07		Vr= 38.88 ✓	Ve= 5.44		Vr= 38.88 ✓	Ve= 6.25		Vr= 38.88 ✓
CZ28 Lnx= 2.50 Lny= 2.50	4.90			4.90			7.12			7.12		
	7.08	+	Mu= 3.71	-6.35	+	Mu= 3.33	8.35	+	Mu= 4.28	-4.29	+	Mu= 2.19
	0.00	+	Ma= 0.00	0.00	+	Ma= 0.00	0.00	+	Ma= 0.00	0.00	+	Ma= 0.00
	3.54			3.54			5.16			5.16		
	Ve= 1.48		Vr= 23.83 ✓	Ve= 1.33		Vr= 23.83 ✓	Ve= 1.71		Vr= 22.69 ✓	Ve= 0.88		Vr= 22.69 ✓
CZ29 Lnx= 2.50 Lny= 2.50	5.17			5.17			7.67			7.67		
	14.71	+	Mu= 5.68	-12.64	+	Mu= 5.68	8.35	+	Mu= 4.28	-4.29	+	Mu= 2.20
	0.01	+	Ma= 0.00	0.00	+	Ma= 0.00	8.35	+	Ma= 5.03	-4.29	+	Ma= 2.58
	3.73			3.73			5.34			5.34		
	Ve= 2.27		Vr= 23.83 ✓	Ve= 2.27		Vr= 23.83 ✓	Ve= 3.72		Vr= 22.69 ✓	Ve= 1.91		Vr= 22.69 ✓
CZ30 Lnx= 2.50 Lny= 2.50	5.52			5.52			7.81			7.81		
	12.64	+	Mu= 6.10	-12.64	+	Mu= 6.10	8.35	+	Mu= 4.28	-4.29	+	Mu= 2.19
	0.01	+	Ma= 0.00	0.00	+	Ma= 0.00	8.35	+	Ma= 5.01	-4.29	+	Ma= 2.57
	3.80			3.80			5.46			5.46		
	Ve= 2.44		Vr= 23.83 ✓	Ve= 2.44		Vr= 23.83 ✓	Ve= 3.72		Vr= 22.69 ✓	Ve= 1.91		Vr= 22.69 ✓
CZ31 Lnx= 2.50 Lny= 2.50	7.73			7.73			5.18			5.18		
	7.92	+	Mu= 4.07	-6.36	+	Mu= 3.26	12.64	+	Mu= 5.71	-12.64	+	Mu= 5.71
	7.08	+	Ma= 4.28	-6.35	+	Ma= 3.84	0.00	+	Ma= 0.00	0.00	+	Ma= 0.00
	5.32			5.32			3.73			3.73		
	Ve= 3.34		Vr= 22.69 ✓	Ve= 2.84		Vr= 22.69 ✓	Ve= 2.29		Vr= 23.83 ✓	Ve= 2.29		Vr= 23.83 ✓
CZ32 Lnx= 2.50 Lny= 2.50	10.34			10.34			10.39			10.39		
	16.71	+	Mu= 8.55	-14.71	+	Mu= 7.53	12.64	+	Mu= 6.48	-12.64	+	Mu= 6.48
	14.71	+	Ma= 7.17	-12.65	+	Ma= 6.16	12.64	+	Ma= 6.22	-12.64	+	Ma= 6.22
	11.39			11.39			11.29			11.29		
	Ve= 6.29		Vr= 38.88 ✓	Ve= 5.48		Vr= 38.88 ✓	Ve= 5.08		Vr= 38.88 ✓	Ve= 5.08		Vr= 38.88 ✓

SHEAR DESIGN CHECK FOR COLUMNS

Column	+X			-X			+Y			-Y		
	Mp	Mc	Mr	Mp	Mc	Mr	Mp	Mc	Mr	Mp	Mc	Mr
C311 Lnx= 2.50 Lny= 2.50	9.57 15.44 + Mu= 8.04 10.41 14.71 + Ma= 7.16 10.98 Ve= 6.08 Vr= 38.88 ✓	9.57 -15.44 + Mu= 8.04 10.41 -14.71 + Ma= 7.16 10.98 Ve= 6.08 Vr= 38.88 ✓	9.68 16.65 + Mu= 8.67 10.52 12.64 + Ma= 6.15 11.11 Ve= 5.93 Vr= 38.88 ✓	9.68 -16.65 + Mu= 8.67 10.52 -12.64 + Ma= 6.15 11.11 Ve= 5.93 Vr= 38.88 ✓								
C312 Lnx= 2.50 Lny= 2.50	4.33 7.08 + Mu= 3.76 4.90 7.08 + Ma= 3.37 5.39 Ve= 2.85 Vr= 23.83 ✓	4.33 -6.35 + Mu= 3.37 4.90 -6.35 + Ma= 3.03 5.39 Ve= 2.56 Vr= 23.83 ✓	6.41 4.29 + Mu= 2.26 7.12 4.29 + Ma= 2.09 7.48 Ve= 1.74 Vr= 22.69 ✓	6.41 -8.35 + Mu= 4.40 7.12 -8.35 + Ma= 4.07 7.48 Ve= 3.39 Vr= 22.69 ✓								
C313 Lnx= 2.50 Lny= 2.50	4.60 14.70 + Mu= 5.17 5.17 14.70 + Ma= 5.17 5.68 Ve= 4.14 Vr= 23.83 ✓	4.60 -12.64 + Mu= 5.17 5.17 -12.64 + Ma= 5.17 5.68 Ve= 4.14 Vr= 23.83 ✓	7.12 6.35 + Mu= 3.29 7.67 4.29 + Ma= 2.09 8.07 Ve= 2.15 Vr= 22.69 ✓	7.12 -8.35 + Mu= 4.33 7.67 -8.35 + Ma= 4.07 8.07 Ve= 3.36 Vr= 22.69 ✓								
C314 Lnx= 2.50 Lny= 2.50	4.82 12.64 + Mu= 5.52 5.52 12.64 + Ma= 5.52 6.20 Ve= 4.42 Vr= 23.83 ✓	4.82 -12.64 + Mu= 5.52 5.52 -12.64 + Ma= 5.52 6.20 Ve= 4.42 Vr= 23.83 ✓	7.31 6.35 + Mu= 3.28 7.81 4.29 + Ma= 2.09 8.20 Ve= 2.15 Vr= 22.69 ✓	7.31 -8.35 + Mu= 4.31 7.81 -8.35 + Ma= 4.08 8.20 Ve= 3.36 Vr= 22.69 ✓								
C315 Lnx= 2.50 Lny= 2.50	7.15 7.92 + Mu= 4.11 7.73 7.92 + Ma= 3.85 8.15 Ve= 3.19 Vr= 22.69 ✓	7.15 -6.36 + Mu= 3.30 7.73 -6.36 + Ma= 3.09 8.15 Ve= 2.56 Vr= 22.69 ✓	4.77 12.64 + Mu= 5.49 5.49 12.64 + Ma= 5.49 6.09 Ve= 4.39 Vr= 23.83 ✓	4.77 -12.64 + Mu= 5.49 5.49 -12.64 + Ma= 5.49 6.09 Ve= 4.39 Vr= 23.83 ✓								
C316 Lnx= 2.50 Lny= 2.50	7.22 7.09 + Mu= 3.67 7.76 7.92 + Ma= 3.86 8.18 Ve= 3.01 Vr= 22.69 ✓	7.22 -6.36 + Mu= 3.29 7.76 -6.36 + Ma= 3.10 8.18 Ve= 2.56 Vr= 22.69 ✓	4.75 12.64 + Mu= 5.43 5.43 12.64 + Ma= 5.43 5.99 Ve= 4.34 Vr= 23.83 ✓	4.75 -12.64 + Mu= 5.43 5.43 -12.64 + Ma= 5.43 5.99 Ve= 4.34 Vr= 23.83 ✓								
C317 Lnx= 2.50 Lny= 2.50	9.54 16.71 + Mu= 10.34 10.34 16.71 + Ma= 8.16 10.83 Ve= 7.40 Vr= 38.88 ✓	9.54 -14.71 + Mu= 7.65 10.34 -14.71 + Ma= 7.18 10.83 Ve= 5.93 Vr= 38.88 ✓	9.58 12.64 + Mu= 6.58 10.39 12.64 + Ma= 6.16 10.93 Ve= 5.09 Vr= 38.88 ✓	9.58 -12.64 + Mu= 6.58 10.39 -12.64 + Ma= 6.16 10.93 Ve= 5.09 Vr= 38.88 ✓								
C318 Lnx= 2.50 Lny= 2.50	9.52 12.65 + Mu= 6.59 10.37 12.65 + Ma= 6.16 10.93 Ve= 5.10 Vr= 38.88 ✓	9.52 -12.65 + Mu= 6.59 10.37 -12.65 + Ma= 6.16 10.93 Ve= 5.10 Vr= 38.88 ✓	9.14 16.70 + Mu= 8.70 9.93 16.70 + Ma= 8.14 10.46 Ve= 6.73 Vr= 38.88 ✓	9.14 -14.70 + Mu= 7.66 9.93 -14.70 + Ma= 7.16 10.46 Ve= 5.93 Vr= 38.88 ✓								
C319 Lnx= 2.50 Lny= 2.50	9.54 16.71 + Mu= 10.33 10.33 16.71 + Ma= 8.16 10.82 Ve= 7.40 Vr= 38.88 ✓	9.54 -14.71 + Mu= 7.65 10.33 -14.71 + Ma= 7.18 10.82 Ve= 5.93 Vr= 38.88 ✓	9.48 12.64 + Mu= 6.59 10.33 12.64 + Ma= 6.16 10.88 Ve= 5.10 Vr= 38.88 ✓	9.48 -12.64 + Mu= 6.59 10.33 -12.64 + Ma= 6.16 10.88 Ve= 5.10 Vr= 38.88 ✓								
C320 Lnx= 2.50 Lny= 2.50	4.32 6.35 + Mu= 3.37 4.89 6.35 + Ma= 3.03 5.37 Ve= 2.56 Vr= 23.83 ✓	4.32 -7.08 + Mu= 3.76 4.89 -7.08 + Ma= 3.37 5.37 Ve= 2.85 Vr= 23.83 ✓	6.40 8.35 + Mu= 4.40 7.13 8.35 + Ma= 4.07 7.49 Ve= 3.39 Vr= 22.69 ✓	6.40 -6.35 + Mu= 3.34 7.13 -6.35 + Ma= 3.09 7.49 Ve= 2.57 Vr= 22.69 ✓								
C321 Lnx= 2.50 Lny= 2.50	4.60 12.65 + Mu= 5.17 5.17 12.65 + Ma= 5.17 5.67 Ve= 4.13 Vr= 23.83 ✓	4.60 -14.70 + Mu= 5.17 5.17 -14.70 + Ma= 5.17 5.67 Ve= 4.13 Vr= 23.83 ✓	7.13 9.06 + Mu= 4.70 7.69 9.06 + Ma= 4.41 8.11 Ve= 3.65 Vr= 22.69 ✓	7.13 -6.35 + Mu= 3.29 7.69 -6.35 + Ma= 3.09 8.11 Ve= 2.55 Vr= 22.69 ✓								
C322 Lnx= 2.50 Lny= 2.50	4.88 12.64 + Mu= 5.60 5.60 12.64 + Ma= 5.60 6.18 Ve= 4.48 Vr= 23.83 ✓	4.88 -12.64 + Mu= 5.60 5.60 -12.64 + Ma= 5.60 6.18 Ve= 4.48 Vr= 23.83 ✓	7.30 8.35 + Mu= 4.32 7.81 8.35 + Ma= 4.07 8.21 Ve= 3.36 Vr= 22.69 ✓	7.30 -6.35 + Mu= 3.28 7.81 -6.35 + Ma= 3.09 8.21 Ve= 2.55 Vr= 22.69 ✓								

SHEAR DESIGN CHECK FOR COLUMNS

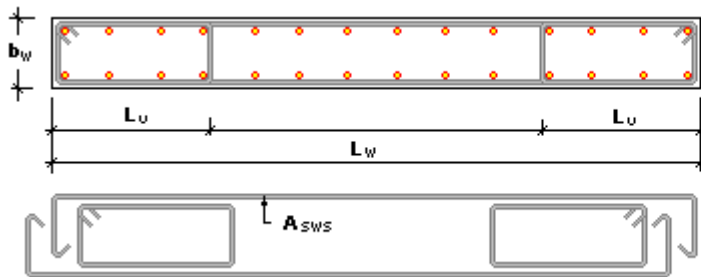
Column	+X			-X			+Y			-Y		
	Mp	Mc	Mr	Mp	Mc	Mr	Mp	Mc	Mr	Mp	Mc	Mr
C413 Lnx= 2.50 Lny= 2.50		3.95			3.95			5.99			5.99	
		14.70	† Mu= 7.90		-12.64	† Mu= 6.80		4.29	† Mu= 2.33		-8.35	† Mu= 4.54
			4.60			4.60			7.12			7.12
		14.70	† Ma= 4.60		-12.64	† Ma= 4.60		6.35	† Ma= 3.06		-8.35	† Ma= 4.02
		5.17			5.17			7.67			7.67	
	Ve= 5.00	Vr= 23.83	✓	Ve= 4.56	Vr= 23.83	✓	Ve= 2.15	Vr= 22.69	✓	Ve= 3.42	Vr= 22.69	✓
C414 Lnx= 2.50 Lny= 2.50		4.06			4.06			6.14			6.14	
		12.64	† Mu= 6.87		-12.64	† Mu= 6.87		4.29	† Mu= 2.33		-8.35	† Mu= 4.54
			4.82			4.82			7.31			7.31
		12.64	† Ma= 4.82		-12.64	† Ma= 4.82		6.35	† Ma= 3.07		-8.35	† Ma= 4.04
		5.52			5.52			7.81			7.81	
	Ve= 4.68	Vr= 23.83	✓	Ve= 4.68	Vr= 23.83	✓	Ve= 2.16	Vr= 22.69	✓	Ve= 3.43	Vr= 22.69	✓
C415 Lnx= 2.50 Lny= 2.50		6.00			6.00			3.95			3.95	
		7.09	† Mu= 3.86		-6.36	† Mu= 3.46		12.64	† Mu= 6.92		-12.64	† Mu= 6.92
			7.15			7.15			4.77			4.77
		7.92	† Ma= 3.81		-6.36	† Ma= 3.06		12.64	† Ma= 4.77		-12.64	† Ma= 4.77
		7.73			7.73			5.49			5.49	
	Ve= 3.07	Vr= 22.69	✓	Ve= 2.61	Vr= 22.69	✓	Ve= 4.68	Vr= 23.83	✓	Ve= 4.68	Vr= 23.83	✓
C416 Lnx= 2.50 Lny= 2.50		6.03			6.03			4.01			4.01	
		7.09	† Mu= 3.86		-6.36	† Mu= 3.46		12.64	† Mu= 6.85		-12.64	† Mu= 6.85
			7.22			7.22			4.75			4.75
		7.09	† Ma= 3.41		-6.36	† Ma= 3.06		12.64	† Ma= 4.75		-12.64	† Ma= 4.75
		7.76			7.76			5.43			5.43	
	Ve= 2.91	Vr= 22.69	✓	Ve= 2.61	Vr= 22.69	✓	Ve= 4.64	Vr= 23.83	✓	Ve= 4.64	Vr= 23.83	✓
C417 Lnx= 2.50 Lny= 2.50		8.49			8.49			8.49			8.49	
		14.71	† Mu= 7.79		-12.65	† Mu= 6.69		12.64	† Mu= 6.70		-12.64	† Mu= 6.70
			9.54			9.54			9.58			9.58
		16.71	† Ma= 9.54		-14.71	† Ma= 7.06		12.64	† Ma= 6.06		-12.64	† Ma= 6.06
		10.34			10.34			10.39			10.39	
	Ve= 6.93	Vr= 38.88	✓	Ve= 5.50	Vr= 38.88	✓	Ve= 5.10	Vr= 38.88	✓	Ve= 5.10	Vr= 38.88	✓
C418 Lnx= 2.50 Lny= 2.50		8.44			8.44			8.19			8.19	
		12.65	† Mu= 6.71		-12.65	† Mu= 6.71		16.70	† Mu= 8.81		-14.70	† Mu= 7.75
			9.52			9.52			9.14			9.14
		12.65	† Ma= 6.06		-12.65	† Ma= 6.06		16.70	† Ma= 8.00		-14.70	† Ma= 7.04
		10.37			10.37			9.93			9.93	
	Ve= 5.11	Vr= 38.88	✓	Ve= 5.11	Vr= 38.88	✓	Ve= 6.73	Vr= 38.88	✓	Ve= 5.92	Vr= 38.88	✓
C419 Lnx= 2.50 Lny= 2.50		8.49			8.49			8.40			8.40	
		16.71	† Mu= 8.84		-14.71	† Mu= 7.78		12.64	† Mu= 6.70		-12.64	† Mu= 6.70
			9.54			9.54			9.48			9.48
		16.71	† Ma= 9.54		-14.71	† Ma= 7.06		12.64	† Ma= 6.05		-12.64	† Ma= 6.05
		10.33			10.33			10.33			10.33	
	Ve= 7.35	Vr= 38.88	✓	Ve= 5.94	Vr= 38.88	✓	Ve= 5.10	Vr= 38.88	✓	Ve= 5.10	Vr= 38.88	✓
C420 Lnx= 2.50 Lny= 2.50		3.74			3.74			5.57			5.57	
		6.35	† Mu= 3.41		-7.08	† Mu= 3.80		8.35	† Mu= 4.47		-4.29	† Mu= 2.29
			4.32			4.32			6.40			6.40
		6.35	† Ma= 2.98		-7.08	† Ma= 3.32		8.35	† Ma= 3.95		-6.35	† Ma= 3.00
		4.89			4.89			7.13			7.13	
	Ve= 2.55	Vr= 23.83	✓	Ve= 2.85	Vr= 23.83	✓	Ve= 3.37	Vr= 22.69	✓	Ve= 2.12	Vr= 22.69	✓
C421 Lnx= 2.50 Lny= 2.50		3.95			3.95			5.99			5.99	
		12.64	† Mu= 6.80		-14.70	† Mu= 7.90		8.35	† Mu= 4.54		-4.29	† Mu= 2.33
			4.60			4.60			7.13			7.13
		12.65	† Ma= 4.60		-14.70	† Ma= 4.60		9.06	† Ma= 4.36		-6.35	† Ma= 3.05
		5.17			5.17			7.69			7.69	
	Ve= 4.56	Vr= 23.83	✓	Ve= 5.00	Vr= 23.83	✓	Ve= 3.56	Vr= 22.69	✓	Ve= 2.15	Vr= 22.69	✓
C422 Lnx= 2.50 Lny= 2.50		4.08			4.08			6.13			6.13	
		12.64	† Mu= 6.89		-12.64	† Mu= 6.88		8.35	† Mu= 4.54		-4.29	† Mu= 2.33
			4.88			4.88			7.30			7.30
		12.64	† Ma= 4.88		-12.64	† Ma= 4.88		8.35	† Ma= 4.03		-6.35	† Ma= 3.07
		5.60			5.60			7.81			7.81	
	Ve= 4.71	Vr= 23.83	✓	Ve= 4.71	Vr= 23.83	✓	Ve= 3.43	Vr= 22.69	✓	Ve= 2.16	Vr= 22.69	✓
C423 Lnx= 2.50 Lny= 2.50		4.10			4.10			6.16			6.16	
		12.64	† Mu= 6.89		-12.64	† Mu= 6.88		8.35	† Mu= 4.54		-4.29	† Mu= 2.33
			4.90			4.90			7.32			7.32
		12.64	† Ma= 4.90		-12.64	† Ma= 4.90		8.35	† Ma= 4.04		-6.35	† Ma= 3.07
		5.62			5.62			7.82			7.82	
	Ve= 4.71	Vr= 23.83	✓	Ve= 4.71	Vr= 23.83	✓	Ve= 3.43	Vr= 22.69	✓	Ve= 2.16	Vr= 22.69	✓
C424 Lnx= 2.50 Lny= 2.50		5.98			5.98			3.95			3.95	
		6.36	† Mu= 3.46		-7.09	† Mu= 3.86		12.64	† Mu= 6.79		-12.64	† Mu= 6.79
			7.14			7.14			4.58			4.58
		6.36	† Ma= 3.05		-7.92	† Ma= 3.81		12.64	† Ma= 4.58		-12.64	† Ma= 4.58
		7.72			7.72			5.14			5.14	
	Ve= 2.60	Vr= 22.69	✓	Ve= 3.06	Vr= 22.69	✓	Ve= 4.55	Vr= 23.83	✓	Ve= 4.55	Vr= 23.83	✓

SHEAR DESIGN CHECK FOR COLUMNS

Column	+X			-X			+Y			-Y		
	Mp	Mc	Mr	Mp	Mc	Mr	Mp	Mc	Mr	Mp	Mc	Mr
C527 Lnx= 2.50 Lny= 2.50	0.00 12.65 8.39 12.65 9.47 7.44	+ Mu= 12.65 + Ma= 5.94	12.65 8.39 5.94 38.88	0.00 -12.65 8.39 -12.65 9.47 7.44	+ Mu= 12.65 + Ma= 5.95	12.65 8.39 5.95 38.88	0.00 12.64 8.19 14.70 9.15 7.83	+ Mu= 12.64 + Ma= 6.94	12.64 8.19 6.94 38.88	0.00 -14.70 8.19 -16.70 9.15 9.04	+ Mu= 14.70 + Ma= 7.89	14.70 8.19 7.89 38.88
C528 Lnx= 2.50 Lny= 2.50	0.00 7.08 3.74 7.08 4.33 4.15	+ Mu= 7.08 + Ma= 3.28	7.08 3.74 3.28 23.83	0.00 -6.35 3.74 -6.35 4.33 3.72	+ Mu= 6.35 + Ma= 2.94	6.35 3.74 2.94 23.83	0.00 8.35 5.57 8.35 6.41 4.89	+ Mu= 8.35 + Ma= 3.88	8.35 5.57 3.88 22.69	0.00 -4.29 5.57 -4.29 6.41 2.51	+ Mu= 4.29 + Ma= 1.99	4.29 5.57 1.99 22.69
C529 Lnx= 2.50 Lny= 2.50	0.00 14.71 3.95 14.71 4.60 8.60	+ Mu= 14.71 + Ma= 6.80	14.71 3.95 6.80 23.83	0.00 -12.64 3.95 -12.64 4.60 7.40	+ Mu= 12.64 + Ma= 5.85	12.64 3.95 5.85 23.83	0.00 8.35 5.99 8.35 7.12 4.87	+ Mu= 8.35 + Ma= 3.82	8.35 5.99 3.82 22.69	0.00 -4.29 5.99 -4.29 7.12 2.50	+ Mu= 4.29 + Ma= 1.96	4.29 5.99 1.96 22.69
C530 Lnx= 2.50 Lny= 2.50	0.00 12.64 4.06 12.64 4.82 7.37	+ Mu= 12.64 + Ma= 5.78	12.64 4.06 5.78 23.83	0.00 -12.64 4.06 -12.64 4.82 7.37	+ Mu= 12.64 + Ma= 5.77	12.64 4.06 5.77 23.83	0.00 8.35 6.14 8.35 7.31 4.87	+ Mu= 8.35 + Ma= 3.81	8.35 6.14 3.81 22.69	0.00 -4.29 6.14 -4.29 7.31 2.50	+ Mu= 4.29 + Ma= 1.96	4.29 6.14 1.96 22.69
C531 Lnx= 2.50 Lny= 2.50	0.00 7.09 6.00 7.09 7.15 4.13	+ Mu= 7.09 + Ma= 3.23	7.09 6.00 3.23 22.69	0.00 -6.36 6.00 -6.36 7.15 3.70	+ Mu= 6.36 + Ma= 2.90	6.36 6.00 2.90 22.69	0.00 12.64 3.95 12.64 4.59 7.39	+ Mu= 12.64 + Ma= 5.84	12.64 3.95 5.84 23.83	0.00 -12.64 3.95 -12.64 4.59 7.39	+ Mu= 12.64 + Ma= 5.84	12.64 3.95 5.84 23.83
C532 Lnx= 2.50 Lny= 2.50	0.00 14.71 8.49 14.71 9.54 8.65	+ Mu= 14.71 + Ma= 6.92	14.71 8.49 6.92 38.88	0.00 -12.65 8.49 -12.65 9.54 7.44	+ Mu= 12.65 + Ma= 5.95	12.65 8.49 5.95 38.88	0.00 12.64 8.49 12.64 9.58 7.43	+ Mu= 12.64 + Ma= 5.94	12.64 8.49 5.94 38.88	0.00 -12.64 8.49 -12.64 9.58 7.43	+ Mu= 12.64 + Ma= 5.94	12.64 8.49 5.94 38.88
C533 Lnx= 2.50 Lny= 2.50	0.00 12.65 8.44 12.65 9.52 7.44	+ Mu= 12.65 + Ma= 5.94	12.65 8.44 5.94 38.88	0.00 -12.65 8.44 -12.65 9.52 7.44	+ Mu= 12.65 + Ma= 5.94	12.65 8.44 5.94 38.88	0.00 12.64 8.19 14.70 9.14 7.83	+ Mu= 12.64 + Ma= 6.95	12.64 8.19 6.95 38.88	0.00 -14.70 8.19 -16.70 9.14 9.04	+ Mu= 14.70 + Ma= 7.89	14.70 8.19 7.89 38.88
C535 Lnx= 2.50 Lny= 2.50	16.36 18.46 17.53 18.46 18.53 7.41	+ Mu= 9.55 + Ma= 8.97	9.55 8.97 88.60	16.36 -21.06 17.53 -21.06 18.53 8.45	+ Mu= 10.89 + Ma= 10.24	10.89 10.24 88.60	130.55 21.39 140.72 23.39 150.34 8.96	+ Mu= 11.10 + Ma= 11.31	11.10 11.31 106.95	130.55 -21.39 140.72 -23.39 150.34 8.96	+ Mu= 11.10 + Ma= 11.31	11.10 11.31 106.95
C635 Lnx= 2.50 Lny= 3.00	0.00 14.15 16.36 18.46 17.53 9.23	+ Mu= 14.15 + Ma= 8.91	14.15 8.91 88.60	0.00 -12.69 16.36 -21.06 17.53 9.14	+ Mu= 12.69 + Ma= 10.17	12.69 10.17 88.60	0.00 0.00 130.55 21.39 140.72 3.43	+ Mu= 0.00 + Ma= 10.29	0.00 0.00 10.29 106.95	0.00 0.00 130.55 -21.39 140.72 3.43	+ Mu= 0.00 + Ma= 10.29	0.00 0.00 10.29 106.95

SHEARWALL DESIGN CHECK

$V_r = A_{ch} (0.65 f_{ctd} + r_{sh} f_{yd})$ Wall shear design
 $V_{rh} = 0.22 f_{cd} A_{ch}$ Max. concrete shear design
 $r_{shx} = A_{sWS} \cdot (\sum L_{etrx}/s) / A_{ch}$ $r_{shy} = A_{sWS} \cdot (\sum L_{etry}/s) / A_{ch}$
 $V_{fr} = \mu N + f_{yd} A_{sd} =$ Working point friction shear force
 $N = N_g - N_e$ Min. Wall load
 $\mu = 1$ (rough surface $\geq 5mm$)



Dikdörtgen perdelerde

$$q_{sh} = \frac{2 \cdot A_{sWS}}{A_{ch}} \cdot \left(\frac{L_w}{s} + \frac{2 \cdot L_u}{s_u} \right)$$

Poligon perdelerde

$$q_{shx} = \frac{A_{sWS}}{A_{ch}} \cdot \left(\sum \frac{L_{etrx}}{s} \right)$$

$$q_{shy} = \frac{A_{sWS}}{A_{ch}} \cdot \left(\sum \frac{L_{etry}}{s} \right)$$

$$V_r = 0.65 \cdot A_{ch} \cdot f_{ctd} + q \cdot A_{ch} \cdot f_{yd} > V_d$$

Column	Dir.	Ln	N	Vd	Vr	Vrh	Vfr	EXPLANATION
CB34	X	2.50	80.844	68.983	200.456	333.667	357.296	✓
	Y	2.50	114.189	72.511	172.934	333.667	390.641	✓
CZ34	X	2.50	64.651	59.369	200.456	333.667	357.972	✓
	Y	2.50	94.758	58.817	172.934	333.667	388.080	✓
C334	X	2.50	52.412	29.806	200.456	333.667	309.470	✓
	Y	2.50	74.158	32.504	172.934	333.667	331.215	✓
C434	X	2.50	38.903	17.687	200.456	333.667	249.599	✓
	Y	2.50	52.734	17.266	172.934	333.667	263.429	✓
C534	X	2.50	22.315	1.336	200.456	333.667	233.010	✓
	Y	2.50	30.728	7.867	172.934	333.667	241.423	✓
C634	X	2.50	4.717	1.109	200.456	333.667	215.413	✓
	Y	3.00	9.240	3.314	172.934	333.667	219.936	✓

(t)